January 2011



REPORT

Noise Impact Assessment Sombra Solar Farm, St. Clair, Ontario

Submitted to:

First Solar Development Canada Attn: Peter Carrie, Vice President 5115 Blackwell Sideroad Sarnia, ON N7T 7H3

REPORT

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NOISE IMPACT ASSESSMENT SOMBRA SOLAR FARM

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1.0 INTRODUCTION

Golder Associates Ltd. (Golder) was retained by First Solar Development Canada Inc. (First Solar) to carry out a Noise Impact Assessment (NIA) in support of the Renewable Energy Approval (REA) application for the Sombra Solar Farm Facility located in St. Clair, Ontario. First Solar, proposes to develop (construct, and operate) the Sombra Solar Farm (Sombra Farm), a renewable energy generation facility with a name plate capacity of up to 20 megawatts (MW).

The Sombra Farm is composed of one (1) 20 MW solar farm that will supply electricity to the local electric grid. Noise sources associated with the solar farm include the transformers, inverters and exhaust fans installed onsite.

An area plan showing the site location and most sensitive Point(s) of Reception (POR(s)) is provided in Figure 1. A site layout plan showing the source locations is provided in Figure 2. A zoning map is provided in Appendix A.

The immediate surroundings of the site are zoned agricultural with isolated dwellings all around and small communities to the west. This area can be best described as Class 3 (Rural) in accordance with MOE guideline publication NPC-232.

For the purpose of this assessment, one hundred and thirteen (113) PORs were selected as being representative of the sensitive receptors in all directions around the site. These receptors are identified as POR001 through POR113. The nearest POR (POR014) is located to the north of the site, approximately 164 m from the nearest source.

For easy comprehension and understanding of this report, acoustical technical terms used in this report are explained in Appendix B.

1.1 Background

On September 24, 2009, Ontario Regulation 359/09 of the Environmental Protection Act received Royal Assent and on October 1, 2009 was filed and came into force. In Ontario, all solar farms were previously assessed using Ontario Ministry of Environment's Noise Pollution Control (NPC) guidelines. O. Reg. 359/09 now contains the current requirements for approval of renewable energy projects under the Renewable Energy Approval (REA) process.

According to the project classification scheme outlined in Part II (Classes of Renewable Energy Generation Facilities), Section 4 of O. Reg. 359/09; the Sombra Solar Farm can be categorized as a Class 3 solar facility. A Class 3 solar facility is defined as a facility of solar panels situated at any location other than mounted on the roof or wall of a building with a name plate capacity greater than 10 kW. Also, O. Reg. 359/09 indicates that a Class 3 solar facility requires a Noise Study Report prepared in accordance with Appendix A of the MOE publication entitled "Basic Comprehensive Certificates of Approval" dated April 2004 and subsequent amendments.

This report has been prepared following the guidelines given in the above noted MOE documentation.





2.0 SITE OPERATIONS

The proposed site is located to the east of Baseline Road and north of Smith Line, in St. Clair, Lambton County, Ontario. Upon final commissioning, the solar farm is expected to supply up to twenty (20) MW of power to the local grid. Noise sources associated with this facility include transformers, inverters and exhaust fans.

Two different scenarios have been considered in this report as described below:

Scenario#1: The Sombra Farm will consist of 20 different transformer stations. Associated with each of transformer stations will be a concrete enclosure. Each enclosure will contain two (2) 500 kW Xantrex inverters with a cooling coil and exhaust opening on the wall for each inverter. There are also two room cooling intakes and two exhausts per enclosure. This scenario provides 9 different sources per transformer station location.

Scenario#2: The Sombra farm will consist of 20 different transformer stations (same location and the same model transformers as above). The two Xantrex model inverters will be replaced by two (2) 500 kW SMA model inverters. There are also two room intakes and two exhausts per enclosure. There are no cooling coil and exhaust openings for the inverters. This scenario provides 5 different sources per transformer station location.

The solar farm will operate year-round during daylight hours. Due to the extended daylight hours during the summer season, it is expected that the facility will also be operating outside of typical daytime hours (i.e., 07:00 hours – 19:00 hours). These noise sources will be situated within the property boundary as shown in Figure 2. For the purpose of this assessment, Golder has conservatively assumed that the equipment will operate at 100% of rated capacity during a predictable worst case hour. A system operation diagram is provided in Appendix C.

The immediate surroundings of the site include agricultural lands with isolated dwellings. Golder has considered this area as Class 3 (Rural) in accordance with MOE publication NPC-232.





3.0 NOISE SOURCE SUMMARY

As discussed, the noise sources of concern associated with this site are the transformers, inverters and exhaust fans. The transformers will be on concrete pads. The inverters will be located inside concrete enclosures as described in Section 2 of this report (i.e., Scenarios #1 and #2). Drawings showing details of the concrete enclosure for both the Xantrex Inverters and the SMA inverters are attached in Appendix D. The Xantrex enclosures will be oriented such that the air intake for the enclosure and openings (intake and exhaust) for the inverters will be on north and south façades and exhaust openings for the enclosure will be on the east façade of each enclosure building. The SMA enclosures will be oriented such that the enclosure intake will be on the east façade and enclosure exhaust openings will be on the north and south façades. Thus the noise sources for each scenario are as follows:

Scenario #1: Xantrex Inverters

Transformer – point source at each transformer station (1 point source per station) Inverter cooling openings - north and south façades (4 vertical area sources per station) Room intake openings - north and south façades (2 vertical area sources per station) Room exhaust fans – two on east façade (2 point sources per station)

Scenario #2: SMA Inverters

Transformer – point source at each transformer station (1 point source per station) Room exhaust openings – north and south façades (2 vertical area sources per station) Room intake openings – two on east façade (2 vertical area sources per station) Noise associated with the inverters are included in the intake and exhaust openings of the enclosure.

In accordance with MOE guidelines, the resulting noise emissions associated with the transformers have been penalised by +5 dB to account for the distinct hum from the transformer coils. Also, based on Golder's noise measurements of the Xantrex inverters, a similar +5 dB penalty has been applied to the noise emissions from the inverters which displayed a tonal character. The same penalty was considered appropriate for the SMA inverters as well. Therefore, all sources associated with this farm include a tonal penalty of +5 dB.

All sources are summarized in Table 3. All source-specific sound pressure levels are summarized in Appendix E.





NOISE IMPACT ASSESSMENT SOMBRA SOLAR FARM

Table 1: Noise Source Summary

Source ID	Source Description	Overall Sound Power Level (dBA)	Source Location	Sound Characteristics	Noise Control Measures
T 0001 – T 020	Transformers	71	0	S,T ¹	U
Scenario #1 – Xantrex Ir	nverters				
C1_001 – C1_020 and C2_001 – C2_020	Enclosure Exhaust Opening for Inverter Cooling	81	О	S,T ¹	U
C3_001 – C3_020 and C4_001 – C4_020	Enclosure Intake Opening for Inverter Cooling	82	О	S,T ¹	U
l1_001 – l1_020 and l2_001 – l2_020	Enclosure Inlet	77	О	S,T ¹	U
E1_001 – E1_020 and E2_001 – E2_020	Exhaust fan	80	Ο	S	U
Scenario #2 – SMA Inve	rters				
E1_001 – E1_020 and E2_001 – E2_020	Enclosure Exhaust Opening ²	75	0	S,T ¹	U
l1_001 - l1_020 and l2_001 - l2_020	Enclosure Inlet ²	67	0	S,T ¹	U

¹ As per MOE guidelines, for tonal sources, the resulting receptor levels have been penalised by 5 dB ² Noise from the inverters is included in the intake and exhaust numbers.

Source Location

O - located/installed outside the building, including on the roof I - located/installed inside the building

- Sound Characteristics S Steady Q Quasi Steady Impulsive I Impulsive
- B Buzzing
- T Tonal
- C Cyclic

Noise Control Measures

- S Silencer, acoustic louver, muffler
- A Acoustic lining, plenum
- B Barrier, berm, or screening
- L Lagging E Acoustic enclosure
- O Other U Uncontrolled



4.0 POINT(S) OF RECEPTION

As discussed previously, a total of 113 PORs were identified, as being potentially impacted by the noise emissions from the proposed Sombra Farm. Among them POR014 has the highest overall levels and is considered in this assessment as the most critical POR.

POR ID	POR Description	Location						
POR001 – POR015, POR113	Residential	Residences to the North and Northeast of the Solar Farm						
POR016 – POR079	Residential	Residences to the Northwest and west of the Solar Farm						
POR080 - POR112	Residential	Residences to the south and southeast of the Solar Farm						

Table 2: Point of Reception Summary



5.0 ASSESSMENT CRITERIA (PERFORMANCE LIMITS)

The proposed solar farm is located in St. Clair, Lambton County, Ontario. The site is surrounded generally by agricultural lands with isolated dwellings all around and community settlement to the west. It is considered that all PORs are located in Class 3 areas.

In predicting the sound level at each POR due to the proposed solar farm, MOE publication NPC-232 requires the application of the principle of "predictable worst case" noise impact. The predictable worst case impact is defined as the largest noise excess produced by the facility over the applicable limit.

The background sound level is considered as traffic noise and other sounds in the area excluding the sound from the facility under assessment. The sound level limit for the residential receptors in a Class 3 area can be described as follows:

The energy averaged sound level (Leq) produced by a source at a receptor location in any one hour period should not exceed the greater of; the energy averaged background sound level in the same hour period, or 45 dBA in the daytime period of 07:00-19:00, or 40 dBA in the evening period of 19:00-23:00 and 40 dBA in the night-time period of 23:00-07:00.

Based on Golder's experience of similar sites, the applicable sound level limits for this site are determined to be the exclusionary minimum sound levels for Class 3 areas as given in table 3.

Time Period	Sound Level Limit for POR in Class 3 Area [dBA]
Day-time (07:00 – 19:00)	45
Evening (19:00 – 23:00)	40
Night-time (23:00 – 07:00)	40

Table 3: Performance Limits for All Points of Reception (PORs)





6.0 IMPACT ASSESSMENT

6.1 Methodology

Sound intensity measurements for the sources were carried out on August 6, 2010 at a solar farm with similar equipment using a Larson Davis 3000+ sound level meter/realtime analyzer equipped with Larson and Davis intensity probe (model 2260). The calibration of the instrumentation was verified before and after the measurements. All measuring equipment used in this study meets the MOE requirements, and calibration certificates are provided in Appendix F.

All relevant sound level measurements taken during the site visit have been documented in 1/3 octave band level format and are summarized in Appendix G. Weather during the August, 2010 site visit included clear conditions with temperatures ranging between 20°C and 24°C. Winds were predominantly from the West at 7 to 17 km/h. Weather data can be found in Appendix H.

The predictions were made using the commercially available software package CadnaA V 4.0.135. Geometrical spreading, attenuation from barriers (if any), ground effect and air absorption were included in the analysis as determined from ISO 9613 (part 2), which is the current standard used for outdoor sound propagation predictions. It should be noted that this standard makes provisions to include a correction to address for downwind or ground based temperature inversion conditions. Conservatively, noise predictions have been made assuming a downwind or moderate temperature inversion conditions for all PORs, a design condition consistent with the accepted practice of the MOE.

All source-specific sound power levels are summarized in Appendix E.

6.2 Results

Tables 4 and 5 summarize the predicted sound pressure levels of Scenario #1 and #2 for each source at the PORs and the distance from each source to the identified PORs. The format for Table 4 and Table 5 are shown below, and the complete tables can be found on the attached CD. Sample calculations are also provided in the attached CD. The predicted results indicate that the sound emissions from the Sombra Farm will meet the MOE noise level limits for Class 3 areas during night-time hours (i.e., 40 dBA).

Figure 3 and 4 show the noise contours for the study area for each scenario considered. Similarly, Tables 6 and 7 provide a summary of the overall predicted noise levels at the identified PORs for each scenario.



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Source ID	POR001		POR002		POR003		POR004		POR005	
	Distance (m)	Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)
T0001										
T0002										
T0003	Refer to attached CD for Table 4.									
T0004										
T0005										

Table 4: Point of Reception Noise Impact – Scenario #1 (Xantrex Inverters)

Table 5: Point of Reception Noise Impact – Scenario #2 (SMA Inverters)

	POR001		POR002		POR003		POR004		POR005	
Source ID	Distance (m)	Overall Sound Pressure Level (dBA)								
T0001										
T0002										
T0003	Refer to att	Refer to attached CD for Table 5.								
T0004										
T0005										



NOISE IMPACT ASSESSMENT SOMBRA SOLAR FARM

Point of reception ID	Point of Reception (POR) Description	Overall SPL at POR (dBA)	Verified by Acoustic Audit (Yes/No)	Performance Limit (dBA)	Compliance with Performance Limit (Yes/No)
POR001 – POR013, POR015, POR113	Residences to the North and Northeast of the Solar Farm	16 – 34	N/A	40	Yes
POR016 – POR079	Residences to the Northwest and west of the Solar Farm	18 - 27	N/A	40	Yes
POR080 – POR112	Residences to the south and southeast of the Solar Farm	4 – 37	N/A	40	Yes

Note: POR014 will be demolished and will not be a POR when the solar farm is operational; Golder's predictive analysis indicates a sound level of 38 dBA at that location.





Point of reception ID	Point of Reception (POR) Description	Overall SPL at POR (dBA)	Verified by Acoustic Audit (Yes/No)	Performance Limit (dBA)	Compliance with Performance Limit (Yes/No)
POR001 – POR013, POR015, POR113	Residences to the North and Northeast of the Solar Farm	9 – 28	N/A	40	Yes
POR016 – POR079	Residences to the Northwest and west of the Solar Farm	12 – 20	N/A	40	Yes
POR080 – POR112	Residences to the south and southeast of the Solar Farm	0 - 30	N/A	40	Yes

Table 7: Acoustic Assessment Summary – Scenario #2 (SMA Inverters)

Note: POR014 will be demolished and will not be a POR when the solar farm is operational; Golder's predictive analysis indicates a sound level of 31 dBA at that location.

For both scenarios, the overall predicted noise levels for all identified PORs, based on site operations, comply with the performance limits for daytime and night-time operations. As a result, no additional mitigation will be required to ensure compliance with MOE noise guidelines.





7.0 CONCLUSIONS

Golder was retained by First Solar Development Canada Inc. to carry out a Noise Impact Assessment for the proposed Sombra Solar Farm located in St. Clair, Ontario. As requested, Golder considered two different scenarios; one with all Xantrex model inverters (2 per station) and the other with all SMA model inverters (two per station). Based on the results presented in this report, the Sombra Solar Farm will operate in compliance with MOE noise guidelines using either Xantrex or SMA inverters.





NOISE IMPACT ASSESSMENT SOMBRA SOLAR FARM

Report Signature Page

Jan la

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LIST OF FIGURES

Figure 1: Area Plan showing Site Location and Points of Reception Figure 2: Site Plan showing Source Locations Figure 3: Results showing Predicted Equivalent Sound Level Contours – Scenario#1

Figure 4: Results showing Predicted Equivalent Sound Level Contours – Scenario#2















Land Use Zoning Plan







APPENDIX B

Description of Technical Terms





DESCRIPTION OF TECHNICAL TERMS

To help understand the analysis and recommendations made in this report, the following is a brief discussion of technical terms.

The strength of a sound source is described in terms of either sound pressure level (SPL) or sound power level (PWL) and are expressed on a logarithmic scale with reference to the lowest possible sound pressure $(2x10^{-5} Pa)$ or power $(10^{-12} W)$ level that human ear can hear. With this appropriate reference parameter the resulting logarithmic scale is referred to as "decibel" (dB). The SPL is thus represented as dB re $2x10^{-5} Pa$ and PWL as dB re $10^{-12}W$.

Since the scale is logarithmic, a source that is twice the strength as another will have a level three decibels (3 dB) higher sound power. SPL attenuates at a rate of 6 dB per doubling of distance.

The sound data and analysis in this report have been given in terms of octave band frequency distribution. Typically, each octave band is expressed in terms of its centre frequency, namely 31. 5, 63, 125, 250, 500, 1000, 2000, 4000 and 8000 Hertz (Hz.).

Human ears are most sensitive in the 500 to 4000 Hz frequency range, above and below this range; the ear is progressively less sensitive to sound. Therefore in order to express sound level more representative of the human hearing response, a weighting is typically applied to each octave band. The most commonly used weighting is called "A-weighting".

It is common practice to express the sound levels over the entire audible spectrum (i.e., 20 Hz to 20 kHz) as an overall sound level (a single number). The overall A-weighted sound level is often used as a criterion to indicate a maximum allowable sound level.

Environmental noise levels vary over time, and are described in terms of one hour energy equivalent sound level, L_{eq} [1 hour]. The Leq is the energy equivalent continuous sound level, which has the same energy as the time varying noise over a prescribed one hour period.





APPENDIX C System Operation Diagram







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APPENDIX D

Concrete Enclosure Details





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REFERENCE STANDARD SPECIFICATION:



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REFERENCE STANDARD SPECIFICATION:

- 1. DWG NO. E-001 ELECTRICAL TYPICAL NOTES, SYMBOLS & ABBREVIATIONS
- DWG NOs. S-301 THRU S-304 TYPICAL PCS BUILDING PLANS AND DETAILS
- DWG NO. E-503 TYP. PCS BLDG. ELECTRICAL EQUIP. ARRANGEMENT PLAN

FIRST SOLAR DEVELOPMENT (CANADA) 5115 BLACKWELL SIDEROAD SARNIA, ONTARIO N7T 7H3	
Elecar Engineering Co. Limited 1149 Venier Rd., Suite 1001 Samia, Ontario N777 376	
SARNIA SOLAR PHOTOVOLTAIC POWER PLANT SITE PLAN CONTROL AGREEMENT	
REV DATE DESCRIPTION Image: Second	
PROJ NO: 5025-0106-22 CAD DWG FILE: E-504 DRAWN BY: GC CHECKED BY:RF SCALE: AS NOTED COPYRIGHT BY: FIRST SOLAR SHEET TITLE TYPICAL PCS BLILL DLAC	
BUILDING SECTION & DETAIL E-504	





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S-300

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REFERENCE NOTES :

DWG NO. E-501 PCS ELECTRICAL EQUIPMENT PLAN.

GENERAL NOTES:

- 1. WORK THIS DWG. WITH THE STANDARD SPECIFICATION.
- 2. VENDOR TO COORDINATE OPENING LOCATIONS WITH ELECTRICAL DRAWINGS
- & VAULT EXTERIOR MEASUREMENTS SHALL MATCH WITH PCS BUILDING EXTERIOR MEASUREMENTS.
- C.S. GUILDING EALERIUM MEASUREMENTS.
 4. VEDIOR STALL PRE-TI/PRE-ASSEMBLE VAULT AND PCS SHELTER AND PROVIDE MATCH MARKINGS TO ASSURE PERFECT ALIGNMENT OF VAULT AND PCS SHELTER ONCE DELIVERED AND ERECTED AT THE JOBSITE.
- JOBSITE. SVENDOR SHALL BE RESPONSIBLE FOR THE LOADING, TRUCKING TO THE JOBSITE, AND COORDINATION WITH THE OWNER DURING THE DEUVERY OF VAULTS AND PCS SHELTER TO THE JOBSITE. OWNER SHALL BE RESPONSIBLE FOR THE SUPPLY OF LIFTING COUPMENT, LABOR AND MISCELLANEOUS TOOLS AND MATERIALS DURING THE UNICADING AND ERECTION OF THE VAULTS AND PCS SHELTER. UNITED SHELTER DURING THE SUPPLY OF
- 7. VENDOR SHALL BE RESPONSIBLE FOR THE FOLLOWING EQUIPMENT AND ACCESSORIES AFTER THE ERECTION OF THE VAULTS AND PCS SHELTER BY THE OWNER, AS
- FOLLOWS: A. INSTALLATION OF SEISMIC/CONNECTING PLATES FOR
- A. INSTALLATION OF SEISMIC/CONNECTING PLATES FOR VAULTS AND SHELTER.
 B. ENGINEER/DESIGN, SUPPLY AND ERECT HVAC UNITS INCLUDING ELECTRICAL HOOK-UPS.
- C. ENGINEER/DESIGN, SUPPLY AND INSTALLATION OF AIR TERMINALS. D. SUPPLY AND INSTALL PATCHING AT DEPRESSIONS
- FOR ALL LIFTING LUG LOCATIONS IN ANY PART OF THE VAULT OR PCS SHELTER AND APPLY FINAL COATINGS OR FINISH SURFACE WITH MATERIAL
- CUATINGS OR FINISH SURFACE WITH MATERIAL SMILAR TO THE ADJACENT AREA. E. SUPPLY AND APPLY SEALANT/MASTIC/CAULKS AT ALL POSSIBLE ENTRY POINTS OF WATER INCLUDING BUT NOT LIMITED TO THE JOINTS BETWEEN THE VAULTS AND THE PCS SHELTER, ATTACHMENT OF EXTERNAL EQUIPMENT AND ACCESSORIES, ETC.

STRUCTURAL DESIGN CRITERIA :

CODE EDITIONS USED - OBC 2006, CAN/CSA-S16-01, CAN/CSA-S136-01 OCCUPANCY GROUP - S-2 OCCUPANCY CATEGORY III TYPE CONSTRUCTION - VB LAND USE ZONE - RENEWABLE ENERGY SQUARE FOOTAGE/ALLOWABLE AREA - 224.25 SF HEIGHT - 11'-6" (APPROX.) ABOVE GRADE OCCUPANT LOAD (PCS) - 1 FLOOR LIVE LOAD - 150 PSF (7.18 kPa) MAXIMUM FLOOR EQUIPMENT LOAD - 6,000 LBS WIND REFERENCE PRESSURES - q50 = 11.5 PSF (0.55 kPa) MAXIMUM |w = 1.25 NET SPECIFIED WIND LOAD - P = 11.8 kN ACTING PERPENDICULAR TO LONG WALL P = 9.7 kN ACTING PERPENDICULAR TO SHORT WALL GROUND SNOW LOADS - 39.2 PSF (1.875 kPa) MAXIMUM BASED ON - Ss = 1.1 kPa, Sr = 0.4 kPa, Is = 1.25 ROOF LIVE LOAD (REDUCEABLE) - 20 PSF SEISMIC DESIGN CRITERIA SITE CLASSIFICATION "C" Ta = 0.2 s IN EACH DIRECTION Fa = 1.0; Fv = 1.0FOR ONTARIO: Sa(0.2) = 0.36, Sa(0.5) = 0.18, Sa(1.0) = 0.063, Sa(2.0) = 0.02 S(T) = 0.36le = 1.5, Mv = 1.0, Rd = 2.0, Ro = 1.3 CONCRETE: F'C = 5,000 PSI @ 28 DAYS REINFORCING STEEL: ASTM A-615, GRADE 60 WIRE MESH: ASTM A-496 OR A-497 7-15-2009 ISSUED FOR CONSTRUCTION C KDK C KDK T B 06-04-2009 UPDATED DRAWING NUMBER A 05-19-2009 ISSUED FOR PROPOSAL REV DATE REVISION DESCRIPTION FINET BOLAR HEI SCHEFTER Buite oct First Solar. . NEW JER FIRST SOLAR DEVELOPMENT (CANADA) 5115 BLACKWELL SIDERDAD SARNIA, ONTARIO N77 7H3 SARNIA SOLAR PHOTOVOLTAIC POWER PLANT SARNIA SOLAR 2 PCS SHELTER FLOOR AND VAULT PLANS DR. BY CHK. BY SCALE: G.C KDK 1/2"=1'-0" NONEMAKER KEITH SYMMERS PROJ. DIRECTOR MARK LANGDON FS ELEC. JOB No: S-301 0 5025-0108-22 THIS PRINT IS NOT TO BE USED FOR CONSTRUCTION UNLESS NOTE AND SIGNED OK FOR CONSTRUCTION ABOVE LAST REVISIOI



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TYPICAL FRONT ELEVATION



D1. WALL CONSTRUCTION: WALL OF THE SHELTER SHALL BE OF PRECAST CONCRETE, THICKNESS SHALL BE DESIGNED BY THE VENDOR BASED FROM THE SPECIFIED DESIGN CRITERIA.

D2. EXTERIOR WALL SHALL BE PLAIN CEMENT FINISHED PAINTED WHITE.

D3. PROVIDE OPENING ON WALLS AS INDICATED.

D4. PROVIDE SEALANT AT ALL JOINTS/CONECTIONS.



TYPICAL LEFT ELEVATION



D3. PROVIDE OPENING ON WALLS AS INDICATED.

D4. PROVIDE SEALANT AT ALL JOINTS/CONECTIONS.

NOTES:

1. SEE DWG S-301 FOR ADDITIONAL NOTES.





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NOTES:

SEE DWG SS-17000-SK-S01 FOR ADDITIONAL NOTES.





















NOTES:

1. SEE DWG S-301 FOR ADDITIONAL NOTES.

PCS FUOOR SLAB, EL. +1'-7"

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A	05-19-2009	ISSUED FOR PROPOSAL	_		G.C	KDK	TZ
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	PC	S SHELTE LAYOUT	R BASE F	RAME G		HP-S-100
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H	-	<u>I P</u> F	<u>10</u> E	<u>INIX</u>		date: 20 APR 2010
709 SIG	MAN R		LE		r	scale: NONE
CONYEF PHONE	⊀S, GA (770) 2	30013 85-3100 FAX (7	770) 285-3076			JOB NUMBER 58820-ED
GAD FILE N/	AME: Sigaron gro	25 TH RI IRV FIRST SOLARIS	TRUCTURAL DRAWINGSISE	820-ED HP-S-100 MA REV 1 DWG-I AY	ΩΠ1	SHEET: 2 OF 5

DESCRIPTION	QTY.	LENGTH	
6" X 14 GA. Z-BRACKET	4	106 1/4	
6" X 14 GA END Z-BRACKET	2	135 3/8	
6" Z-BRACKET SPLICE PLATE	2	10	
3 1/2" X 5 1/8" 16GA C-ROOF BOW	10	135 1/4	
3" X 16 GA STRIPS	3	120	
3" X 16 GA STRIPS	3	92 1/4	
4 1/2" WALL POST X 14 GA	11	112 7/8	
4 1/2" WALL POST X 14 GA	2	50 1/2"	
4 1/2" WALL POST X 14 GA	2	99 5/16"	
4 1/2" WALL POST X 14 GA	2	98 5/16"	
4 1/2" WALL POST X 14 GA	12	111 7/8	
4 1/2" WALL POST X 14 GA	4	24 1/4	
4 1/2" WALL POST X 14 GA	1	8 1/4	
4 1/2" WALL POST X 14 GA	2	46 3/8	
2 1/8" X 4 1/2" WALL POST X 14 GA	1	13 5/8	100
4 1/2" WALL POST X 14 GA	2	112 1/2	
4 1/2" WALL POST X 14 GA	1	8 7/8	
7" \			
5 X 4 1/2 WALL POST X 14 GA	1	112 1/8	101
3 X 4 1/2 WALL POST X 14 GA	1	112 5/16	101
2 3/8 x 4 1/2 WALL POST X 14 GA	2	111 //8	
7 3/16" WALL POST X 14 GA	1	111 7/8	
/ 3/16" WALL POST X 14 GA	1	112 5/8	
4" WALL POST X 14 GA	1	99 5/16"	
4 WALL POST X 14 GA	1	98 5/16"	
3 WALL POST X 14 GA	1	50 1/2	
2 7/8 WALL POST X 14 GA	1	110 7/16	
2 1/2" WALL POST X 14 GA	1	111 7 /9	100
3 1/2" WALL POST X 14 GA	1	112 7/16	100
4 1/2" X 2 1/8" DOOR POST	1	112 1/16	
4 1/2" X 2 1/8" DOOR POST	1	112 7/16	100
4 1/2"X2 1/8" DOOR HEADER-14 GA	1	44"	100
EXHAUST PLENUMS, INVERTER BTM REAR-14 GA	2	5 7/8 X 50 7/16	100
PAN SP-1 & FIRER OPTIC CHASE FILLER	1	26 15/16249 6/16	100
20 X 32 7 /8 PAIN HOOD TOP W/DIPD SOPEEN	0	20 13/10/43 0/10	100
20 X 32 7/8 RAIN HOOD DOP W/DIRD SCREEN		32 7/0	
20 X 32 7/8 RAIN HOUD BIM W/BIRD SCREEN	4	32 //8	10C
12 x 5/ 1/2 RAIN HOOD W/BUG SCREEN	2	5/ 1/2	100
FILTER FRAME PANEL, 14 GA.	2	24 1/16 X 51 1/4	100
Z-BRKT, FILTER FRAME, 14 GA.	4	23 3/8	100
HAT-SHAPED BRKT, FILTER FRAME, 14 GA.	2	23 13/16	100
FILTER END COVER, 14 GA.	2	50 1/2	100
17X3X16 WIREWAY W/(3) CUTOUTS	1	17X3X16	101
17X12X55 7/8 WIREWAY W/CUTOUT	1	55 7/8	101
16X15X73 7/8 WIREWAY W/(3) CO	1	73 7/8	101
SUPPORT, EXT. WIREWAY	1	36X31 7/16	101
STD 1" WALL & ROOF INSULATION W/SOLID L PUEBLO TAN EMBOSSED ALUM. WALL & ROOF	INERS SKINS	1	
SID. 5/8" OSB WAFFERBOARD ROOF UNDERL	AYMENT		J



	REVISION RECORD								
REV	DATE	BY	DESCRIPTION						
\triangle	20 APR 2010	GC	RELEASED FOR PRODUCTION						
Λ	30 JUL 2010	GC	REMOVED RAILING & LIGHTNING PROTECT. ADDED SPLICE BOX & XFMR LOCK. CHGD XFMR SIZE & WW LAYOUT						
<u>/</u> 2	18 AUG 2010	GC	ADDED NOTE FOR IPLASTIC INSULATION BUSHINGS.						
\wedge									



48"

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3'-6<u>11</u>" -2'-3<u>15</u>" -

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12'-13"

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ATTACH (2) PCS NEOPRENE GASK INSIDE WALL OF FILTER FRAME H 2 PL. E ASSY ED: 2	5 OF 2 TTO THE ALF.
PROJECT PROJECT # 5032-0101-23	
	TIL RURY 5
PRODUCT # S-T-M-1-CEC-3-1-SS-	-0-0-1.0
PCS-M4	
DRAWING TITLE	DRAWING #
PCS SHELTER FILTER FRAME ASSEMBLY	HP-S-100
FIRST SOLAR	drawn by: GC
	ENG. APPROVAL:
HIIPHOENIX	20 APR 2010 SCALE:
709 SIGMAN ROAD CONYERS, GA 30013	Y NONE
	2002U-EU Sheet: 1111 5 OF 5
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Estimated Source PWL from Measurement data, dB re. $20x10^{-12}$ W



Description	Data Source	31.5	63	125	250	500	1000	2000	4000	8000	dBA
Pauwels 1000 kVA 27600Y/15935 2X 208Y/120 Transformer	Measured (Appendix G)	71	74	72	71	68	64	60	61	57	70
Xantrex Inverter Enclosure	Measured (Appendix G)	84	81	84	85	85	84	80	75	85	89
SMA Inverter	Measured (Appendix G)	80	81	75	79	79	73	75	77	72	83







West Caldwell Calibration Laboratories Inc.

Certificate of Calibration

for

Manufactured By: Model No.: Serial No.: Calibration Recall No.:

CALIBRATOR BRUEL & KJAER 4230 565639 : C6270

Submitted by:

Customer:

Company: Address: Golder Associates Ltd.

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Specification No.

4230 B&K (see attached)

Upon receipt for Calibration, the instrument was found to be:

Within (X) see attached Report of Calibration

the tolerance of the indicated specification.

West Caldwell Calibration Laboratories' calibration control system meets the following requirements, ISO 10012-1 MIL-STD- 45662A, ANSI/NCSL, Z540-1, IEC Guide 25, ISO 9001:2000 and ISO/IEC 17025:2005

Note: With this Certificate, Report of Calibration is included.

Calibration Date: 08 March 2007

Certificate No: C6270 -4

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

Approved by:

Stanley Christopher Quality Manager



220 Rutherford Rd. S., Unit 210, Brampton, Ontario L6W 3J6 Canada

ISO 9001:2000 Registered Company Calibration Traceable To N. I. S. T.



Phone: (905) 595-1107

Fax: (905) 595-1108

CERTIFICATE of CALIBRATION

Make :	PCB Piezotronics	Reference # :	88771
Model :	377A60A	Customer :	Golder Associates Ltd Mississauga, ON
Descr. :	Microphone		.,
Serial # :	1022	P. Order :	Stefan

Cal. status : Received in spec's, no adjustment made. Tested with L&D LS3000+ s# 182

JOLA Instruments Inc. certifies that the above listed instrument was calibrated on date noted and was released from this laboratory performing in accordance with the specifications set forth by the manufacturer.

Unless otherwise noted in the calibration report a 4:1 accuracy ratio was maintained for this calibration.

Our calibration system complies with the requirements of ISO-17025 standard, working standards used for calibration are certified by or traceable to the National Research Council of Canada or the National Institute of Standards and Technology.

Calibrated : Jan 06, 2009

Asset # : MS000008

By:

Cal. Due : Jan 06, 2010

J. Raposo

Temperature : 23 °C \pm 2 °C Relative Humidity : 45 % \pm 20 %

Standards used : J-129 J-163 J-216

JOLA Instruments Inc.

REPAIR AND CALIBRATION TRACEABLE TO NRC AND NIST

88 Judge Rd. Toronto, ON, M8Z 5B4 Phone : 416 234 0354

Fax: 416 234 9562

http: // www.jola.com e-Mail: jola @ jola.com

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Certificate of Calibration and Conformance

Certificate Number 2009-120808

Instrument Model 2260, Serial Number 0263, was calibrated on 04AUG2009. The instrument meets factory specifications per Procedure D0001.8089.

New Instrument Date Calibrated: 04AUG2009 Calibration due:

Calibration Standards Used

MANUFACTURER	MODEL	SERIAL NUMBER	INTERVAL	CAL. DUE	TRACEABILITY NO.
Hewlett Packard	34401A	US36015216	12 Months	06MAY2010	4342531
Larson Davis	LDSigGn / 2209	0097 / 0118	12 Months	20JUL2010	2009-120295

Reference Standards are traceable to the National Institute of Standards and Technology (NIST)

Calibration Environmental Conditions

Temperature: 24 ° Centigrade

Relative Humidity: 29 %

Affirmations

This Certificate attests that this instrument has been calibrated under the stated conditions with Measurement and Test Equipment (M&TE) Standards traceable to the U.S. National Institute of Standards and Technology (NIST). All of the Measurement Standards have been calibrated to their manufacturers' specified accuracy / uncertainty. Evidence of traceability and accuracy is on file at Provo Engineering & Manufacturing Center. An acceptable accuracy ratio between the Standard(s) and the item calibrated has been maintained. This instrument meets or exceeds the manufacturer's published specification unless noted.

This calibration complies with the requirements of ISO 17025 and ANSI Z540. The collective uncertainty of the Measurement Standard used does not exceed 25% of the applicable tolerance for each characteristic calibrated unless otherwise noted.

The results documented in this certificate relate only to the item(s) calibrated or tested. A one year calibration is recommended, however calibration interval assignment and adjustment are the responsibility of the end user. This certificate may not be reproduced, except in full, without the written approval of the issuer.

Signed: 6

Preamplifier Model: 2260-Low Serial Number: 0263 Certificate of Electrical Conformance

Frequency response of this model 2260-Low preamplifier was tested at a level of 1 Vrms with 18pF microphone capacitance and driving a short cable. Output level at 1kHz is 0.8914 Vrms (-0.999 dBV), uncertainty 0.033 dB. Results are displayed relative to the level at 1kHz.



2.51	-16.84	0.075	n/a n/a	630.96	-0.01	0.010	+0.10, -0.11
3 16	-15.07	0.058	n/a n/a	794.33	-0.00	0.016	+0.10, -0.11
3 98	-13 28	0.058	n/a n/a	1000.00	0.00	0.016	+0.11, -0.10
5 01	-11 47	0.036	n/a n/a	1258.90	0.00	0.016	+0.11, -0.10
6 21	_9 71	0.036	n/a n/a	1584.90	0.01	0.016	+0.12, -0.10
7 94	-8 01	0.036	n/a n/a	1995.30	0.01	0.016	+0.12, -0.10
10.00	-6.42	0.000	n/a n/a	2511.90	0.01	0.016	+0.12, -0.10
10.00	-0.42	0.016	n/a n/a	3162.30	0.01	0.016	+0.13, -0.10
12.59	~4.33	0.016	n/a n/a	3981 10	0.01	0.016	+0.13, -0.10
15.85	-3.75	0.010	-1 20 -5 00	5011 90	0 00	0.016	+0.14, -0.10
19.95	-2.73	0.016	-1.20, -3.00	6309 60	-0.01	0.016	+0.14, -0.11
25.12	-1.95	0.010	-0.50 -2.20	7943 30	-0.03	0.016	+0.14, -0.13
31.62	-1.34	0.016	-0.30, -2.20	10000 00	-0.07	0.016	+0.14, -0.16
39.81	-0.92	0.016	-0.32, -1.50	12590.00	-0.07	0.016	n/a n/a
50.12	-0.62	0.016	-0.21, -1.05	12589.00	-0.11	0.016	n/a n/a
63.10	-0.43	0.016	-0.11, -0.75	15849.00	-0.20	0.016	n/a n/a
79.43	-0.29	0.016	-0.05, -0.52	19953.00	-0.33	0.010	n/a n/a
100.00	-0.20	0.016	+0.00, -0.37	25250.00	-0.54	0.022	
125.89	-0.14	0.016	+0.03, -0.30	31500.00	-0.84	0.022	n/a n/a
158.49	-0.10	0.016	+0.05, -0.25	39750.00	-1.32	0.022	n/a n/a
199.53	-0.07	0.016	+0.07, -0.21	50000.00	-2.00	0.022	n/a n/a
251.19	-0.05	0.016	+0.08, -0.18	63000.00	-2.93	0.047	n/a n/a
316.23	-0.04	0.016	+0.09, -0.16	79500.00	-4.12	0.047	n/a n/a
398.11	-0.03	0.016	+0.09, -0.14	100000.00	-5.51	0.047	n/a n/a
501.19	-0.02	0.016	+0.10, -0.12	126000.00	-7.10	0.063	n/a n/a

Noise floor data: 1kHz (1/3 Octave) = 0.60 uV, -4.4 dBuV, uncertainty = 0.47 dB Flat (20Hz-20kHz) = 5.0 uV, 13.9 dBuV, uncertainty = 0.47 dB Awt = 2.7 uV, 8.7 dBuV, uncertainty = 0.46 dB

Uncertainties are given as expanded uncertainty at ~95% confidence interval (k = 2).

Technician: Jason Grace Test Date: 04AUG2009

Preamplifier Model: 2260-High Serial Number: 0263 Certificate of Electrical Conformance

Frequency response of this model 2260-High preamplifier was tested at a level of 1 Vrms with 18pF microphone capacitance and driving a short cable. Output level at 1kHz is 0.9005 Vrms (-0.910 dBV), uncertainty 0.033 dB. Results are displayed relative to the level at 1kHz.



Freq (Hz)	Measured (dB)	Uncert (dB)	Tolerance (dB)	Freq (Hz)	Measured (dB)	Uncert (dB)	Tolerance (dB)
2.51	-16.94	0.075	n/a n/a	630.96	-0.01	0.016	+0.10, -0.11
3.16	-15.12	0.058	n/a n/a	794.33	-0.01	0.016	+0.10, -0.11
3.98	-13.29	0.058	n/a n/a	1000.00	0.00	0.016	+0.11, -0.10
5.01	-11.46	0.036	n/a n/a	1258.90	0.00	0.016	+0.11, -0.10
6.31	-9.67	0.036	n/a n/a	1584.90	0.01	0.016	+0.12, -0.10
7.94	-7.96	0.036	n/a n/a	1995.30	0.01	0.016	+0.12, -0.10
10.00	-6.37	0.016	n/a n/a	2511.90	0.01	0.016	+0.12, -0.10
12.59	-4.94	0.016	n/a n/a	3162.30	0.01	0.016	+0.13, -0.10
15.85	-3.70	0.016	n/a n/a	3981.10	0.01	0.016	+0.13, -0.10
19,95	-2.69	0.016	-1.20, -5.00	5011.90	0.00	0.016	+0.14, -0.10
25.12	-1.90	0.016	-0.73, -3.30	6309.60	-0.01	0.016	+0.14, -0.11
31.62	-1.32	0.016	-0.50, -2.20	7943.30	-0.03	0.016	+0.14, -0.13
39.81	-0.90	0.016	-0.32, -1.50	10000.00	-0.06	0.016	+0.14, -0.16
50.12	-0.61	0.016	-0.21, -1.05	12589.00	-0.11	0.016	n/a n/a
63.10	-0.42	0.016	-0.11, -0.75	15849.00	-0.20	0.016	n/a n/a
79.43	-0.29	0.016	-0.05, -0.52	19953.00	-0.32	0.016	n/a n/a
100.00	-0.20	0.016	+0.00, -0.37	25250.00	-0.53	0.022	n/a n/a
125.89	-0.14	0.016	+0.03, -0.30	31500.00	-0.83	0.022	n/a n/a
158.49	-0.10	0.016	+0.05, -0.25	39750.00	-1.29	0.022	n/a n/a
199.53	-0.07	0.016	+0.07, -0.21	50000.00	-1.96	0.022	n/a n/a
251 19	-0.05	0.016	+0.08, -0.18	63000.00	-2.88	0.047	n/a n/a
316.23	-0.04	0.016	+0.09, -0.16	79500.00	-4.05	0.047	n/a n/a
398.11	-0.03	0.016	+0.09, -0.14	100000.00	-5.43	0.047	n/a n/a
501.19	-0.02	0.016	+0.10, -0.12	126000.00	-7.01	0.063	n/a n/a

Noise floor data: 1kHz (1/3 Octave) = 0.62 uV, -4.1 dBuV, uncertainty = 0.47 dB Flat (20Hz-20kHz) = 5.2 uV, 14.3 dBuV, uncertainty = 0.47 dB Awt = 2.8 uV, 9.0 dBuV, uncertainty = 0.46 dB

Uncertainties are given as expanded uncertainty at ~95% confidence interval (k = 2).

Technician: Jason Grace Test Date: 04AUG2009

Model: 2260-Phase Serial Number: 0263 CH 1 Mic: 2640 1436 CH 2 Mic: 2640 1345

Phase errors for the probe. This Class 1 Intensity Probe was tested with a Residual-intensity calibrator model CAL 291. This data was taken after the probe was adjusted for phase with the two adjustors on the side of the probe handle.



Freq (Hz)	Measured (degree)	LD Tolerance (degree)	Spacer (mm)	Freq (Hz)	Measured (degree)	LD Tolerance (degree)	Spacer (mm)
50.12	0.0000	+0.1047, -0.1047	50	631.00	0.0200	+0.1711, -0.1711	12
63.10	-0.0100	+0.1318, -0.1318	50	794.30	0.0350	+0.2153, -0.2153	12
79.43	-0.0150	+0.1660, -0.1660	50	1000.00	0.0500	+0.2711, -0.2711	12
100.00	-0.0200	+0.2089, -0.2089	50	1259.00	0.0550	+0.3413, -0.3413	12
125.90	-0.0250	+0.0631, -0.0631	12	1585.00	0.1000	+0.4297, -0.4297	12
158.50	-0.0200	+0.0681, -0.0681	12	1995.00	0.1000	+0.5409, -0.5409	12
199.50	-0.0100	+0.0681, -0.0681	12	2512.00	0.1500	+0.6810, -0.6810	12
251.20	-0.0100	+0.0681, -0.0681	12	3162.00	0.2000	+0.8574, -0.8574	12
316 20	-0.0100	+0.0857, -0.0857	12	3981.00	0.2500	+1.0800, -1.0800	12
398.10	0.0000	+0.10790.1079	12	5012.00	0.3050	+1.3590, -1.3590	12
501.20	0.0100	+0.1359, -0.1359	12				

Limits are the smallest of ANSI S1.9-1996 table 7 or IEC 1043-1993 table 2 Class 1.

Technician: Jason Grace Test Date: 04AUG2009



APPENDIX G

Measurements

(Measured sound pressure level (L_{EQ}) in one third octave band format is given in this appendix. The data are given in dB re 20 x 10⁻⁶ Pa. The measurements were taken as a scan of the surface)



Frequency (Hz)	Transformer	Transformer	Transformer	Xantrex Intake	Xantrex Exhaust	Xantrex Cooling1	Xantrex Cooling2	SMA intake	SMA exhaust	
25	51	52 51		72	75	68	70	55	69	
31.5	52	55	52	66	72	63	68	55	69	
40	50	51	50	62	70	65	68	59	76	
50	50	53	51	59	69	64	67	62	75	
63	56	58	58	65	67	67	70	58	74	
80	51	48	45	65	66	69	71	55	73	
100	53	50	44	66	65	69	71	55	71	
125	56	55	58	73	73	72	73	61	66	
160	46	41	37	68	70	70	70	55	65	
200	55	45	39	70	65	72	73	51	63	
250	53	54	51	74	66	71	75	56	69	
315	51	48	45	74	74	72	78	64	76	
400	51	50	47	72	78	70	73	57	74	
500	52	51	44	70	69	68	70	61	70	
630	46	47	41	69	69	68	70	56	71	
800	47	46	37	74	69	74	76	52	66	
1000	50	40	36	65	66	67	70	53	63	
1250	44	38	35	69	67	68	73	54	68	
1600	45	38	35	69	67	67	72	54	67	
2000	41	35	34	63	66	64	71	52	63	
2500	45	37	39	60	64	62	69	54	71	
3150	48	37	44	58	63	59	67	55	75	
4000	32	33	28	56	61	57	65	46	59	
5000	36	42	40	61	58	59	66	45	57	
6300	43	39	40	78	62	76	81	55	70	
8000	34	34	34	59	52	59	66	42	56	
10000	34	31	29	50	44	51	55	41	55	



APPENDIX H

Weather Data



Weather Data Source: Station:

Environment Canada, Climate Data Online, <u>www.climate.weatheroffice.ec.gc.ca/climateData/canada_e.html</u> LONDON INT'L AIRPORT Latitude: 43° 1.8' N Longitude: 82° 9' W

	-	_				-		-		-									-	-	_	-	_	-	_
Weather		Clear	Clear	Mainly Clear	Mostly Cloudy	Mainly Clear	Mostly Cloudy	Mostly Cloudy	Mainly Clear	Mostly Cloudy	Mainly Clear	Mostly Cloudy	Mainly Clear	Mainly Clear	Mainly Clear	Mainly Clear	Clear	Clear							
Wind Chill																									
Stn Press	(кРа)	97.61	97.65	97.67	97.67	97.68	97.74	97.76	97.81	97.85	97.90	97.90	97.92	97.91	97.86	97.82	97.81	97.81	97.86	97.87	97.92	97.99	98.10	98.12	98.15
Visibility	(km)	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24	24
Wind Spd	(km/h)	13	9	4	7	7	9	4	9	6	7	7	13	15	17	17	24	15	15	13	17	11	7	6	6
Wind Dir	(10's deg)	34	29	32	29	32	34	32	31	35	28	28	29	26	27	27	28	31	31	31	33	26	1	36	3
Rel Hum	(%)	78	81	84	81	68	71	73	71	62	60	52	53	62	52	50	53	54	54	55	58	62	67	71	78
Dew Point	Temp (°C)	15	15	14	14	12	12	12	13	12	12	12	12	15	13	13	14	14	14	13	12	11	11	11	11
Temp (°C)		19	18	17	17	18	17	17	18	19	20	22	22	23	23	24	24	24	24	22	21	19	17	16	14
Time		00:00	1:00	2:00	3:00	4:00	5:00	6:00	00:2	8:00	00:6	10:00	11:00	12:00	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00
Date/Time		8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010	8/6/2010

At Golder Associates we strive to be the most respected global group of companies specializing in ground engineering and environmental services. Employee owned since our formation in 1960, we have created a unique culture with pride in ownership, resulting in long-term organizational stability. Golder professionals take the time to build an understanding of client needs and of the specific environments in which they operate. We continue to expand our technical capabilities and have experienced steady growth with employees now operating from offices located throughout Africa, Asia, Australasia, Europe, North America and South America.

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