December 2010



REPORT

Noise Impact Assessment Moore Solar Farm, St. Clair, Ontario

Submitted to:

First Solar Development Canada Attn: Peter Carrie, Vice President 5115 Blackwell Sideroad Sarnia, ON N7T 7H3

REPORT

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Table of Contents

1.0	INTRO	DUCTION	1
	1.1	Background	1
2.0	SITE O	PERATIONS	2
3.0	NOISE	SOURCE SUMMARY	3
4.0	POINT(S) OF RECEPTION	5
5.0	ASSES	SMENT CRITERIA (PERFORMANCE LIMITS)	6
6.0		T ASSESSMENT	7
	6.1	Methodology	
	6.2	Results	7
7.0	CONCL	.USIONS1	1

TABLES

Table 1: Noise Source Summary	4
Table 2: Point of Reception Summary	5
Table 3: Performance Limits for All Points of Reception (PORs)	6
Table 4: Point of Reception Noise Impact – Scenario #1 (Xantrex Inverters)	8
Table 5: Point of Reception Noise Impact – Scenario #2 (SMA Inverters)	8
Table 6: Acoustic Assessment Summary – Scenario #1 (Xantrex Inverters)	9
Table 7: Acoustic Assessment Summary – Scenario #2 (SMA Inverters)1	0

FIGURES

Figure 1: Area Plan showing Site Location and Points of Reception	. 13
Figure 2: Site Plan showing Source Locations	. 13
Figure 3: Results showing Predicted Equivalent Sound Level Contours – Scenario#1	. 13
Figure 4: Results showing Predicted Equivalent Sound Level Contours – Scenario#2	. 13





APPENDICES

APPENDIX A Land Use Zoning Plan

APPENDIX B Description of Technical Terms

APPENDIX C System Operation Diagram

APPENDIX D Concrete Enclosure Details

APPENDIX E Source Sound Levels

APPENDIX F Equipment Calibration

APPENDIX G Measurements

APPENDIX H Weather Data



1.0 INTRODUCTION

Golder Associates Ltd. (Golder) was retained by First Solar Development Canada Inc. (First Solar) to carry out a Noise Impact Assessment (NIA) in support of the Renewable Energy Approval (REA) application for the Moore Solar Farm Facility located in St. Clair, Ontario. First Solar, proposes to develop (construct, and operate) the Moore Solar Farm (Moore Farm), a renewable energy generation facility with a name plate capacity of up to 20 megawatts (MW).

The Moore Farm is composed of one (1) 20 MW solar farm that will supply electricity to the local electric grid. Noise sources associated with the solar farm include the transformers, inverters and exhaust fans installed onsite.

An area plan showing the site location and most sensitive Point(s) of Reception (POR(s)) is provided in Figure 1. A site layout plan showing the source locations is provided in Figure 2. A zoning map is provided in Appendix A.

The immediate surroundings of the site include agricultural land uses with isolated dwellings and a small community to the northwest. This area can be best described as Class 3 (Rural) in accordance with MOE guideline publication NPC-232.

For the purpose of this assessment, fifty-one (51) PORs were selected as being representative of the sensitive receptors in all directions around the site. These receptors are identified as POR001 through POR051. The nearest POR (POR043) is located to the south-west of the site, approximately 590 m from the nearest source.

For easy comprehension and understanding of this report, acoustical technical terms used in this report are explained in Appendix B.

1.1 Background

On September 24, 2009, Ontario Regulation 359/09 of the Environmental Protection Act received Royal Assent and on October 1, 2009 was filed and came into force. In Ontario, all solar farms were previously assessed using Ontario Ministry of Environment's Noise Pollution Control (NPC) guidelines. O. Reg. 359/09 now contains the current requirements for approval of renewable energy projects under the Renewable Energy Approval (REA) process.

According to the project classification scheme outlined in Part II (Classes of Renewable Energy Generation Facilities), Section 4 of O. Reg. 359/09; the Moore Solar Farm can be categorized as a Class 3 solar facility. A Class 3 solar facility is defined as a facility of solar panels situated at any location other than mounted on the roof or wall of a building with a name plate capacity greater than 10 kW. Also, O. Reg. 359/09 indicates that a Class 3 solar facility requires a Noise Study Report prepared in accordance with Appendix A of the MOE publication entitled "Basic Comprehensive Certificates of Approval" dated April 2004 and subsequent amendments.

This report has been prepared following the guidelines given in the above noted MOE documentation.





2.0 SITE OPERATIONS

The proposed site is located on the northwest corner of Rokeby Line and King's Highway No. 40, in St. Clair, Lambton County, Ontario. Upon final commissioning, the solar farm is expected to supply up to twenty (20) MW of power to the local grid. Noise sources associated with this facility include transformers, inverters and exhaust fans.

Two different scenarios have been considered in this report as described below:

Scenario#1: The Moore Farm will consist of 20 different transformer stations. Associated with each of transformer stations will be a concrete enclosure. Each enclosure will contain two (2) 500 kW Xantrex inverters with a cooling coil and exhaust opening on the wall for each inverter. There are also two room cooling intakes and two exhausts per enclosure. This scenario provides 9 different sources per transformer station location.

Scenario#2: The Moore farm will consist of 20 different transformer stations (same location and the same model transformers as above). The two Xantrex model inverters will be replaced by two (2) 500 kW SMA model inverters. There are also two room intakes and two exhausts per enclosure. There are no cooling coil and exhaust openings for the inverters. This scenario provides 5 different sources per transformer station location.

The solar farm will operate year-round during daylight hours. Due to the extended daylight hours during the summer season, it is expected that the facility will also be operating outside of typical daytime hours (i.e., 07:00 hours – 19:00 hours). These noise sources will be situated within the property boundary as shown in Figure 2. For the purpose of this assessment, Golder has conservatively assumed that the equipment will operate at 100% of rated capacity during a predictable worst case hour. A system operation diagram is provided in Appendix C.

The immediate surroundings of the site include agricultural lands with isolated dwellings. Golder has considered this area as Class 3 (Rural) in accordance with MOE publication NPC-232.





3.0 NOISE SOURCE SUMMARY

As discussed, the noise sources of concern associated with this site are the transformers, inverters and exhaust fans. The transformers will be on concrete pads. The inverters will be located inside concrete enclosures as described in Section 2 of this report (i.e., Scenarios #1 and #2). Drawings showing details of the concrete enclosure for both the Xantrex Inverters and the SMA inverters are attached in Appendix D. The Xantrex enclosures will be oriented such that the air intake for the enclosure and openings (intake and exhaust) for the inverters will be on north and south façades and exhaust openings for the enclosure will be on the east façade of each enclosure building. The SMA enclosures will be oriented such that the enclosure intake will be on the east façade and enclosure exhaust openings will be on the north and south façades. Thus the noise sources for each scenario are as follows:

Scenario #1: Xantrex Inverters

Transformer – point source at each transformer station (1 point source per station) Inverter cooling openings - north and south façades (4 vertical area sources per station) Room intake openings - north and south façades (2 vertical area sources per station) Room exhaust fans – two on east façade (2 point sources per station)

Scenario #2: SMA Inverters

Transformer – point source at each transformer station (1 point source per station) Room exhaust openings – north and south façades (2 vertical area sources per station) Room intake openings – two on east façade (2 vertical area sources per station) Noise associated with the inverters are included in the intake and exhaust openings of the enclosure.

In accordance with MOE guidelines, the resulting noise emissions associated with the transformers have been penalised by +5 dB to account for the distinct hum from the transformer coils. Also, based on Golder's noise measurements of the Xantrex inverters, a similar +5 dB penalty has been applied to the noise emissions from the inverters which displayed a tonal character. The same penalty was considered appropriate for the SMA inverters as well. Thus all sources associated with this farm include a tonal penalty of +5 dB.

All sources are summarized in Table 3. All source-specific sound pressure levels are summarized in Appendix E.





NOISE IMPACT ASSESSMENT **MOORE SOLAR FARM**

Table 1: Noise Source Summary

Source ID	Source Description	Overall Sound Power Level (dBA)	Source Location	Sound Characteristics	Noise Control Measures
T 0001 – T 020	Transformers	71	0	S,T ¹	U
Scenario #1 – Xantrex II	nverters				
C1_001 – C1_020 and C2_001 – C2_020	Enclosure Exhaust Opening for Inverter Cooling	81	О	S,T ¹	U
C3_001 – C3_020 and C4_001 – C4_020	Enclosure Intake Opening for Inverter Cooling	82	О	S,T ¹	U
l1_001 – l1_020 and l2_001 – l2_020	Enclosure Inlet	77	Ο	S,T ¹	U
E1_001 – E1_020 and E2_001 – E2_020	Exhaust fan	80	Ο	S	U
Scenario #2 – SMA Inve	rters				
E1_001 – E1_020 and E2_001 – E2_020	Enclosure Exhaust Opening ²	75	Ο	S,T ¹	U
l1_001 – l1_020 and l2_001 – l2_020	Enclosure Inlet ²	67	Ο	S,T ¹	U

¹ As per MOE guidelines, for tonal sources, the resulting receptor levels have been penalised by 5 dB ² Noise from the inverters is included in the intake and exhaust numbers.

Source Location

O - located/installed outside the building, including on the roof I - located/installed inside the building

Sound Characteristics

- S Steady Q Quasi Steady Impulsive I Impulsive
- B Buzzing
- T Tonal
- C Cyclic

Noise Control Measures

- S Silencer, acoustic louver, muffler
- A Acoustic lining, plenum
- B Barrier, berm, or screening
- L Lagging E Acoustic enclosure
- O Other U Uncontrolled



4.0 POINT(S) OF RECEPTION

As discussed previously, a total of 51 PORs were identified, as being potentially impacted by the noise emissions from the proposed Moore Farm. Among them POR043 has the highest overall levels and is considered in this assessment as the most critical POR.

POR IDPOR DescriptionLocationPOR001 - POR 039ResidentialResidences to the Northwest of the Solar FarmPOR040 - POR 044ResidentialResidences to the Southwest of the Solar FarmPOR045 - POR 051ResidentialResidences to the Southeast of the Solar Farm

Table 2: Point of Reception Summary





5.0 ASSESSMENT CRITERIA (PERFORMANCE LIMITS)

The proposed solar farm is located in St. Clair, Ontario. The site is surrounded generally by agricultural and industrial lands with isolated dwellings all around and community settlement to the northwest. It is considered that all PORs are located in Class 3 areas.

In predicting the sound level at each POR due to the proposed solar farm, MOE publication NPC-232 requires the application of the principle of "predictable worst case" noise impact. The predictable worst case impact is defined as the largest noise excess produced by the facility over the applicable limit.

The background sound level is considered as traffic noise and other sounds in the area excluding the sound from the facility under assessment. The sound level limit for the residential receptors in a Class 3 area can be described as follows:

The energy averaged sound level (Leq) produced by a source at a receptor location in any one hour period should not exceed the greater of; the energy averaged background sound level in the same hour period, or 45 dBA in the daytime period of 07:00-19:00, or 40 dBA in the evening period of 19:00-23:00 and 40 dBA in the night-time period of 23:00-07:00.

Based on Golder's experience of similar sites, the applicable sound level limits for this site are determined to be the exclusionary minimum sound levels for Class 3 areas as given in table 3.

Time Period	Sound Level Limit for POR in Class 3 Area [dBA]
Day-time (07:00 – 19:00)	45
Evening (19:00 – 23:00)	40
Night-time (23:00 – 07:00)	40

Table 3: Performance Limits for All Points of Reception (PORs)





6.0 IMPACT ASSESSMENT

6.1 Methodology

Sound intensity measurements for the sources were carried out on August 6, 2010 at a solar farm with similar equipment using a Larson Davis 3000+ sound level meter/realtime analyzer equipped with Larson and Davis intensity probe (model 2260). The calibration of the instrumentation was verified before and after the measurements. All measuring equipment used in this study meets the MOE requirements, and calibration certificates are provided in Appendix F.

All relevant sound level measurements taken during the site visit have been documented in 1/3 octave band level format and are summarized in Appendix G. Weather during the August, 2010 site visit included clear conditions with temperatures ranging between 20°C and 24°C. Winds were predominantly from the West at 7 to 17 km/h. Weather data can be found in Appendix H.

The predictions were made using the commercially available software package CadnaA V 4.0.135. Geometrical spreading, attenuation from barriers (if any), ground effect and air absorption were included in the analysis as determined from ISO 9613 (part 2), which is the current standard used for outdoor sound propagation predictions. It should be noted that this standard makes provisions to include a correction to address for downwind or ground based temperature inversion conditions. Conservatively, noise predictions have been made assuming a downwind or moderate temperature inversion conditions for all PORs, a design condition consistent with the accepted practice of the MOE.

All transformers were modelled as point sources. In scenario #1 all inverter related sources were modelled as point sources and vertical area sources, while in scenario #2 the inverter related sources were modelled as vertical area sources only.

All source-specific sound power levels are summarized in Appendix E.

6.2 Results

Tables 4 and 5 summarize the predicted sound pressure levels of Scenario #1 and #2 for each source at the PORs and the distance from each source to the identified PORs. The format for Table 4 and Table 5 are shown below, and the complete tables can be found on the attached CD. Sample calculations are also provided in the attached CD. The predicted results indicate that the sound emissions from the Moore Farm will meet the MOE noise level limits for Class 3 areas during night-time hours (i.e., 40 dBA).

Figure 3 and 4 show the noise contours for the study area for each scenario considered. Similarly, Tables 6 and 7 provide a summary of the overall predicted noise levels at the identified PORs for each scenario.



and a state of the	
P 4' 16	

	POR001		POR002		POR003		POR004		POR005	
Source ID	Distance (m)	Overall Sound Pressure Level (dBA)								
T0001		-		-		-	-		-	
T0002										
T0003	Refer to att	ached CD for Ta	able 4.							
T0004										
T0005										

Table 4: Point of Reception Noise Impact – Scenario #1 (Xantrex Inverters)

Table 5: Point of Reception Noise Impact – Scenario #2 (SMA Inverters)

Source IDDistance (m)Sound PressureDistance (m)Sound Distance (m)Distance PressureSound (m)		POR004		POR005						
		Sound Pressure		Sound Pressure		Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)	Distance (m)	Overall Sound Pressure Level (dBA)
T0001		-	-	-		-	<u>-</u>	-	<u>-</u>	-
T0002										
T0003	Refer to att	ached CD for Ta	able 5.							
T0004										
T0005										





NOISE IMPACT ASSESSMENT MOORE SOLAR FARM

Table 6: Acoustic Assessment Summary – Scenario #1 (Xantrex Inverters)

Point of reception ID	Point of Reception (POR) Description	Overall SPL at POR (dBA)	Verified by Acoustic Audit (Yes/No)	Performance Limit (dBA)	Compliance with Performance Limit (Yes/No)
POR001 – POR 039	Residences to the Northwest of the Solar Farm	19 – 21	N/A	40	Yes
POR040 – POR 044	Residences to the Southwest of the Solar Farm	22 – 28	N/A	40	Yes
POR045 – POR 051	Residences to the Southeast of the Solar Farm	15 - 26	N/A	40	Yes





NOISE IMPACT ASSESSMENT MOORE SOLAR FARM

Point of reception ID	Point of Reception (POR) Description	Overall SPL at POR (dBA)	Verified by Acoustic Audit (Yes/No)	Performance Limit (dBA)	Compliance with Performance Limit (Yes/No)
POR001 – POR 039	Residences to the Northwest of the Solar Farm	12 – 14	N/A	40	Yes
POR040 – POR 044	Residences to the Southwest of the Solar Farm	15 – 21	N/A	40	Yes
POR045 – POR 051	Residences to the Southeast of the Solar Farm	7 - 18	N/A	40	Yes

Table 7: Acoustic Assessment Summary – Scenario #2 (SMA Inverters)

For both scenarios, the overall predicted noise levels for all identified PORs, based on site operations, comply with the performance limits for daytime and night-time operations. As a result, no additional mitigation will be required to ensure compliance with MOE noise guidelines.





7.0 CONCLUSIONS

Golder was retained by First Solar Development Canada Inc. to carry out a Noise Impact Assessment for the proposed Moore Solar Farm located in St. Clair, Ontario. As requested, Golder considered two different scenarios; one with all Xantrex model inverters (2 per station) and the other with all SMA model inverters (two per station). Based on the results presented in this report, it is concluded that the Moore Solar Farm will operate in compliance with MOE noise guidelines using either Xantrex or SMA inverters.





NOISE IMPACT ASSESSMENT MOORE SOLAR FARM

Report Signature Page

Ja la

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Joe Tomaselli M.Eng., P.Eng Associate

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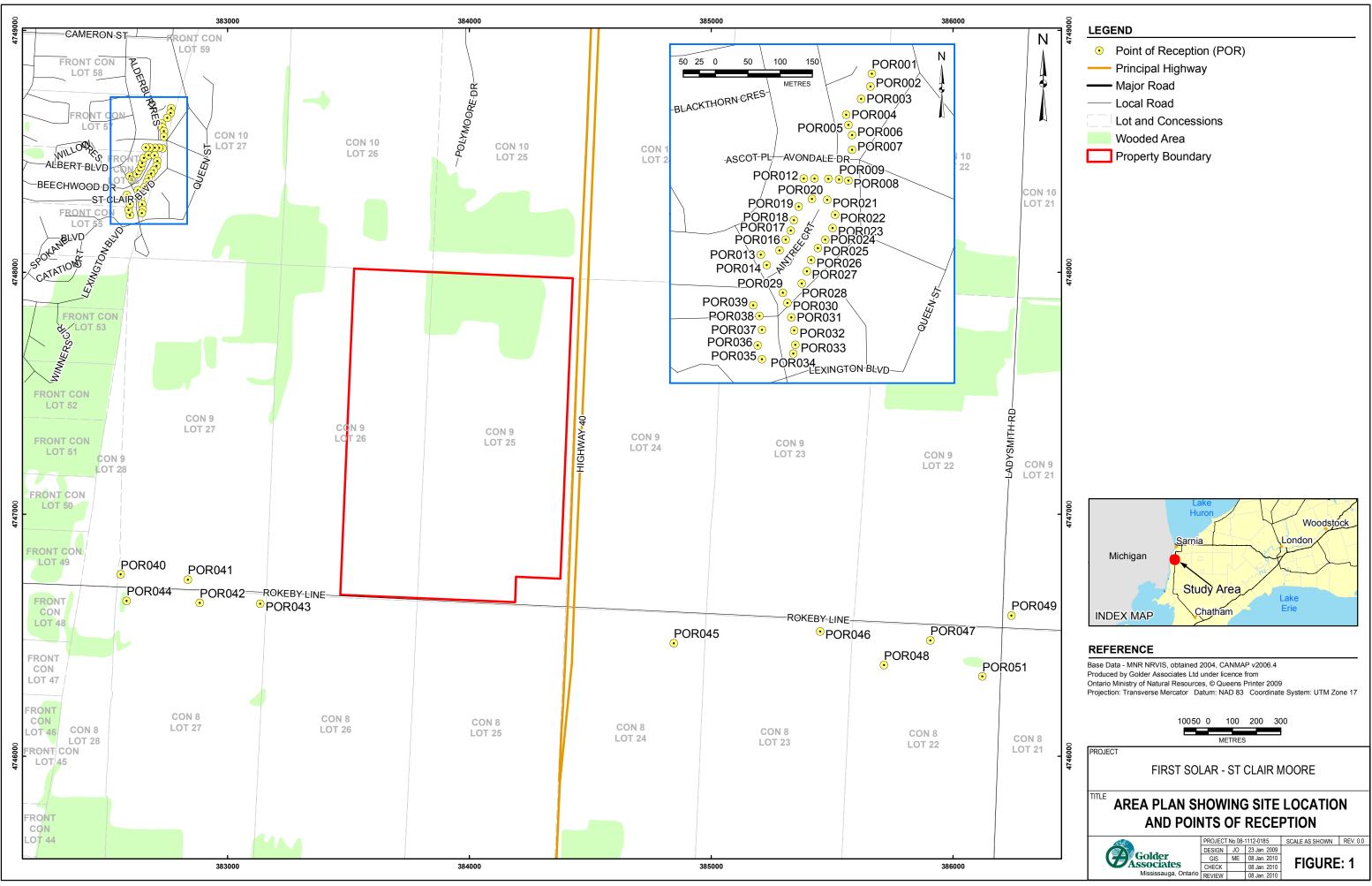


LIST OF FIGURES

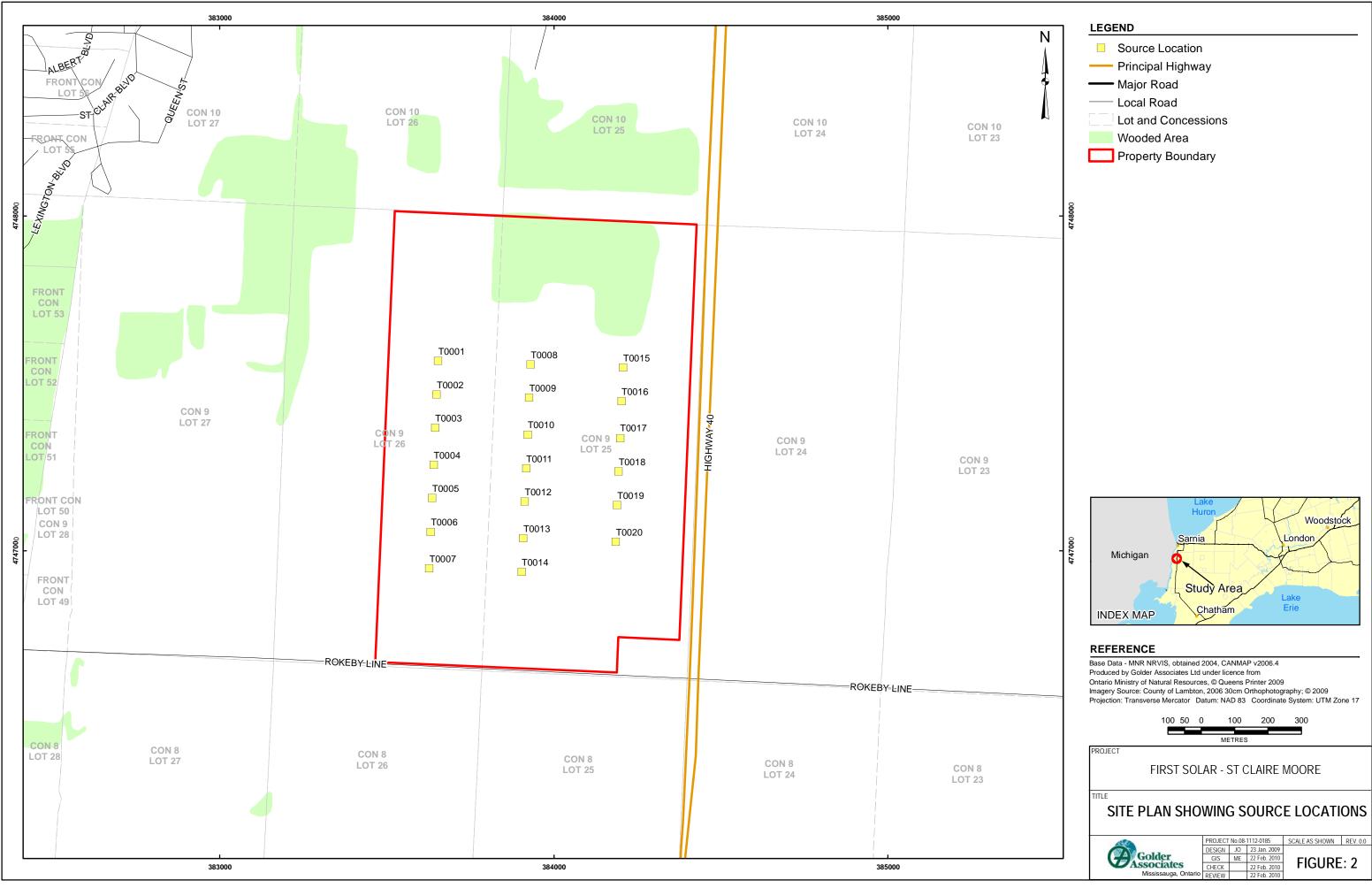
Figure 1: Area Plan showing Site Location and Points of Reception Figure 2: Site Plan showing Source Locations Figure 3: Results showing Predicted Equivalent Sound Level Contours – Scenario#1

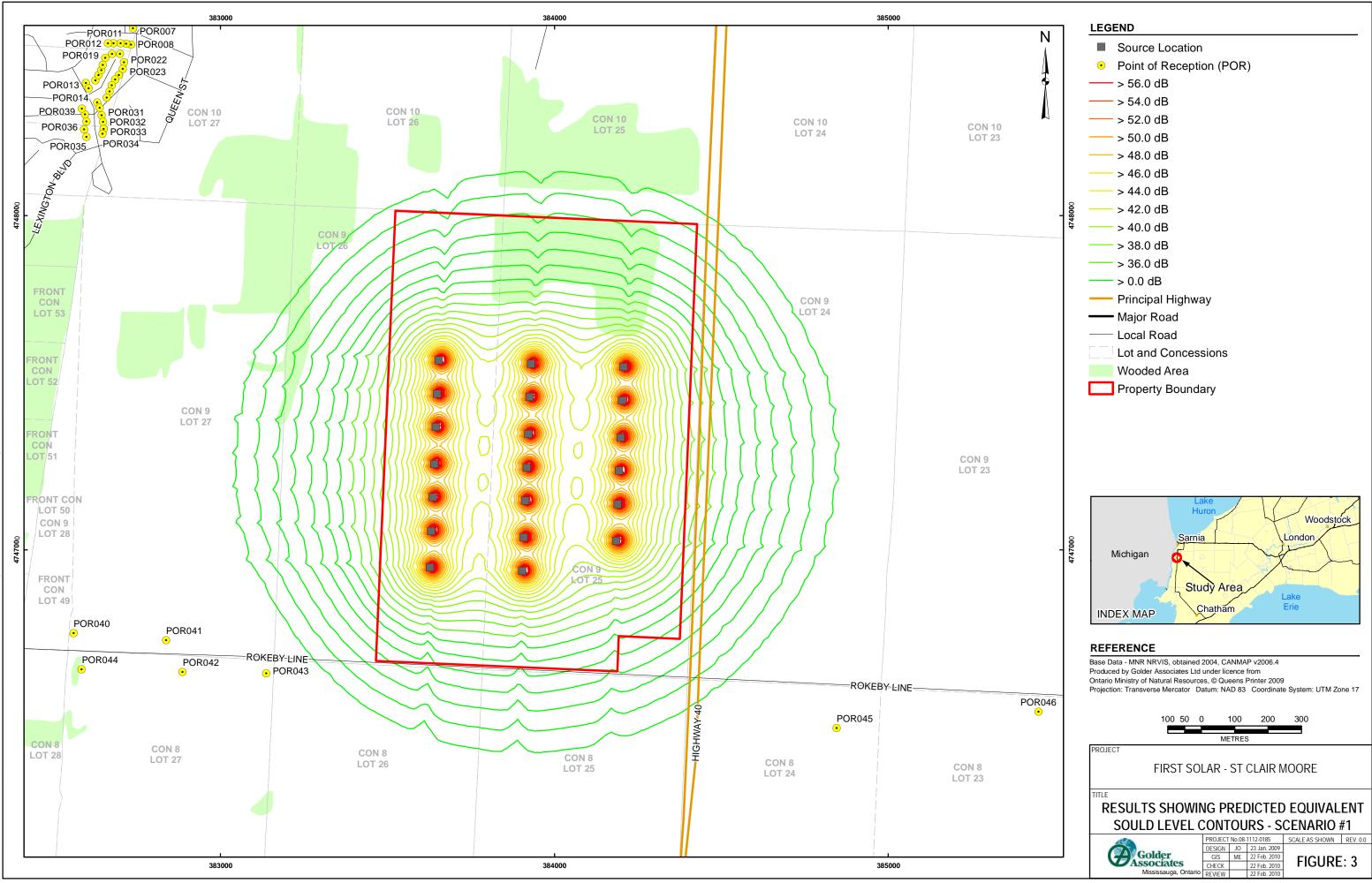
Figure 4: Results showing Predicted Equivalent Sound Level Contours – Scenario#2

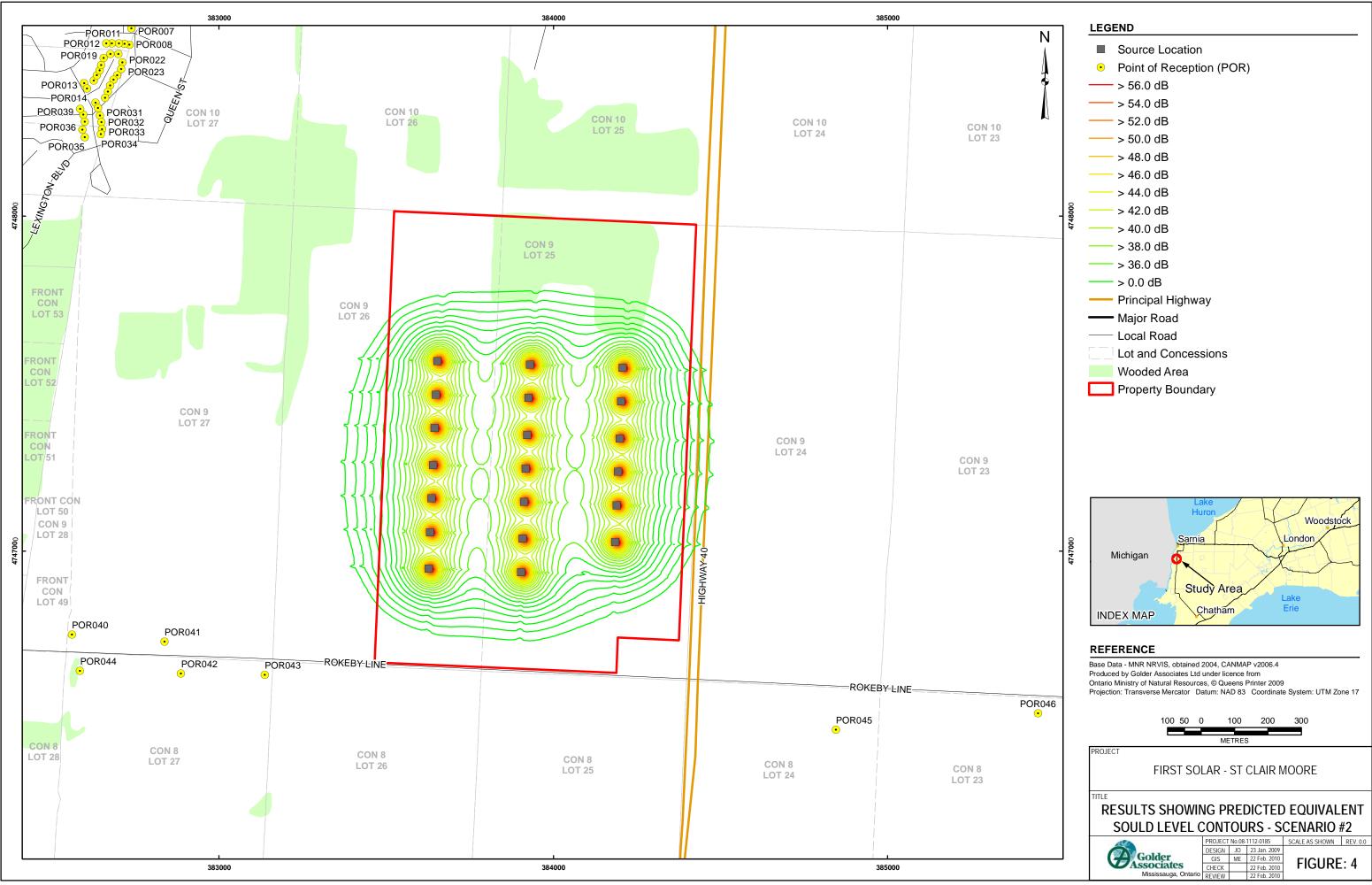




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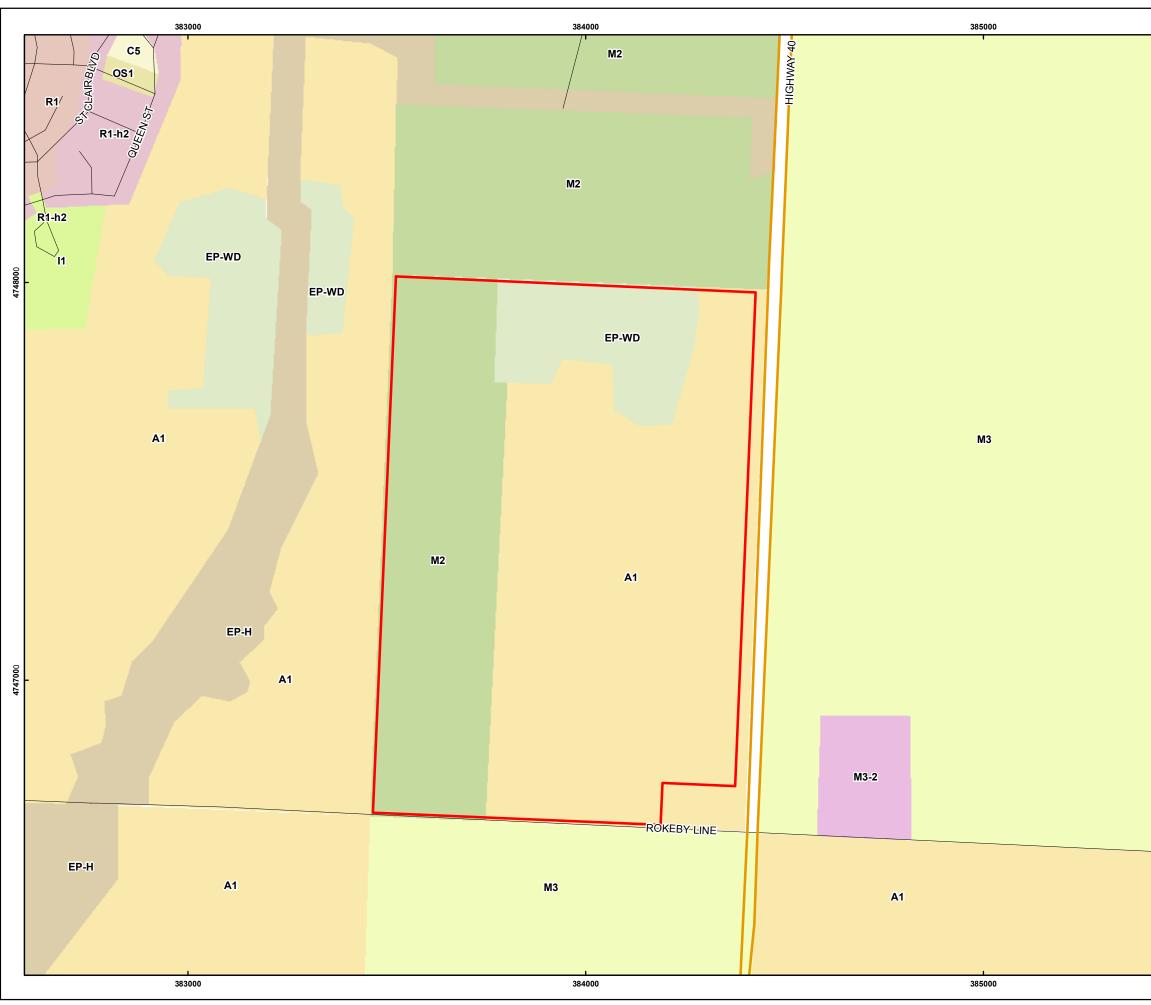




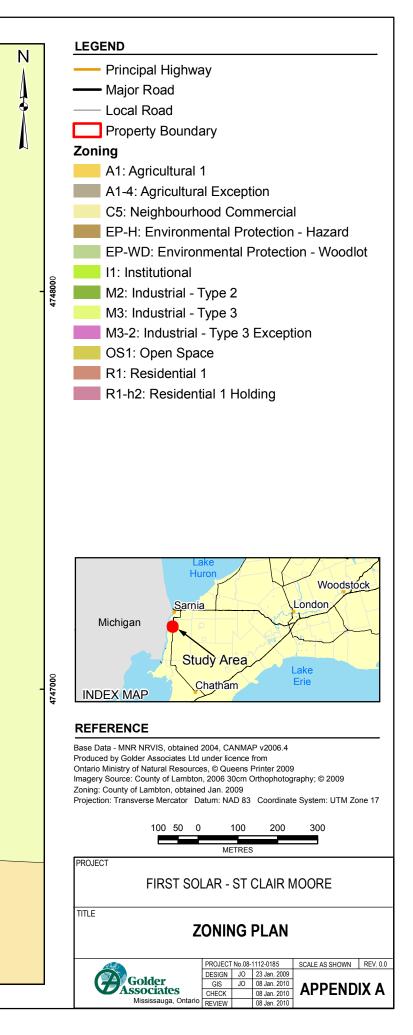


Land Use Zoning Plan





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APPENDIX B

Description of Technical Terms





DESCRIPTION OF TECHNICAL TERMS

To help understand the analysis and recommendations made in this report, the following is a brief discussion of technical terms.

The strength of a sound source is described in terms of either sound pressure level (SPL) or sound power level (PWL) and are expressed on a logarithmic scale with reference to the lowest possible sound pressure $(2x10^{-5} Pa)$ or power $(10^{-12} W)$ level that human ear can hear. With this appropriate reference parameter the resulting logarithmic scale is referred to as "decibel" (dB). The SPL is thus represented as dB re $2x10^{-5} Pa$ and PWL as dB re $10^{-12}W$.

Since the scale is logarithmic, a source that is twice the strength as another will have a level three decibels (3 dB) higher sound power. SPL attenuates at a rate of 6 dB per doubling of distance.

The sound data and analysis in this report have been given in terms of octave band frequency distribution. Typically, each octave band is expressed in terms of its centre frequency, namely 31. 5, 63, 125, 250, 500, 1000, 2000, 4000 and 8000 Hertz (Hz.).

Human ears are most sensitive in the 500 to 4000 Hz frequency range, above and below this range; the ear is progressively less sensitive to sound. Therefore in order to express sound level more representative of the human hearing response, a weighting is typically applied to each octave band. The most commonly used weighting is called "A-weighting".

It is common practice to express the sound levels over the entire audible spectrum (i. e., 20 Hz to 20 kHz) as an overall sound level (a single number). The overall A-weighted sound level is often used as a criterion to indicate a maximum allowable sound level.

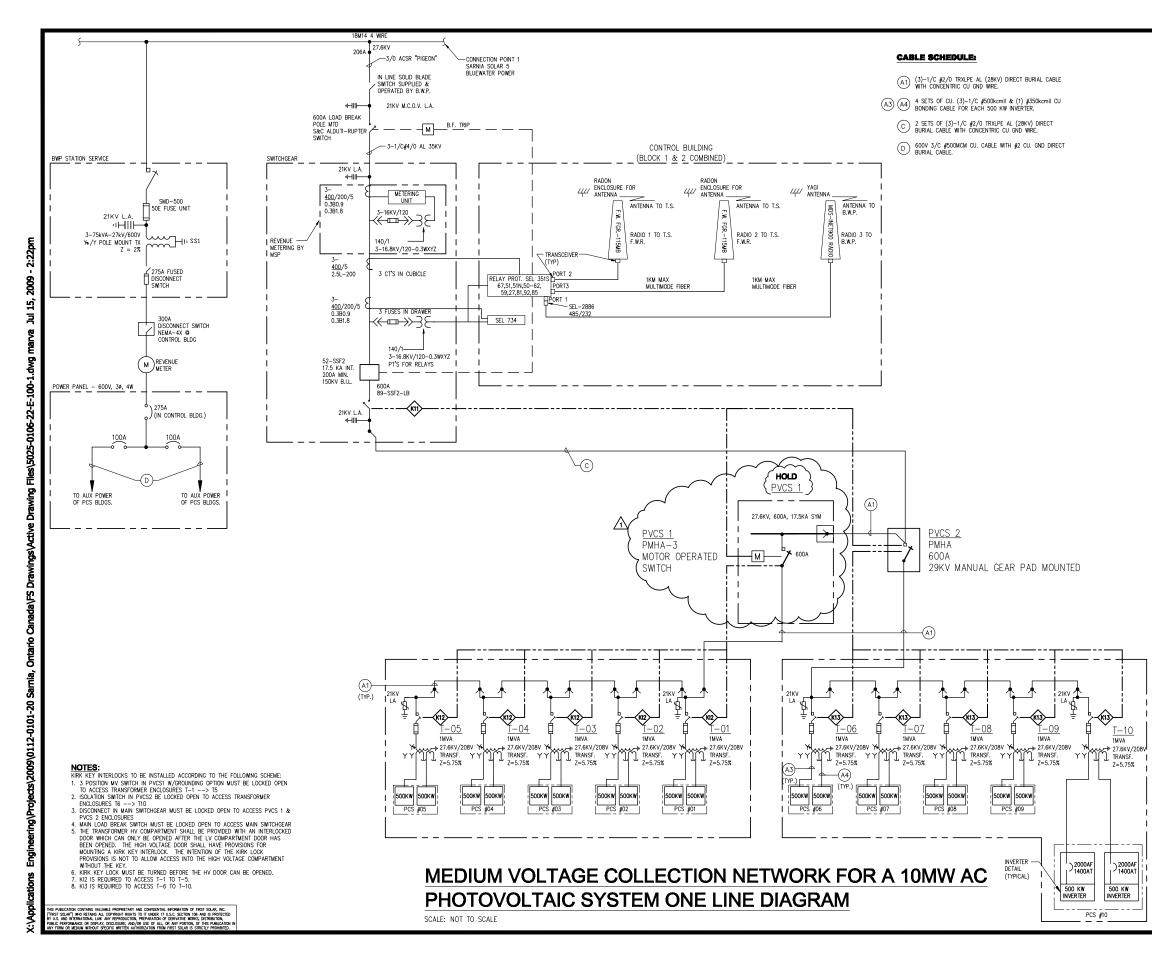
Environmental noise levels vary over time, and are described in terms of one hour energy equivalent sound level, L_{eq} [1 hour]. The Leq is the energy equivalent continuous sound level, which has the same energy as the time varying noise over a prescribed one hour period.

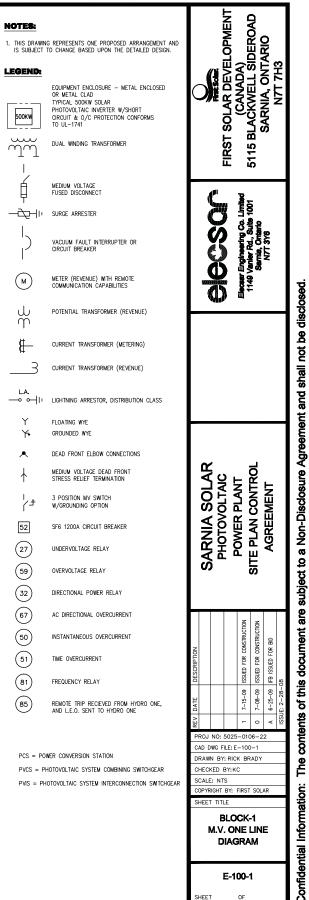




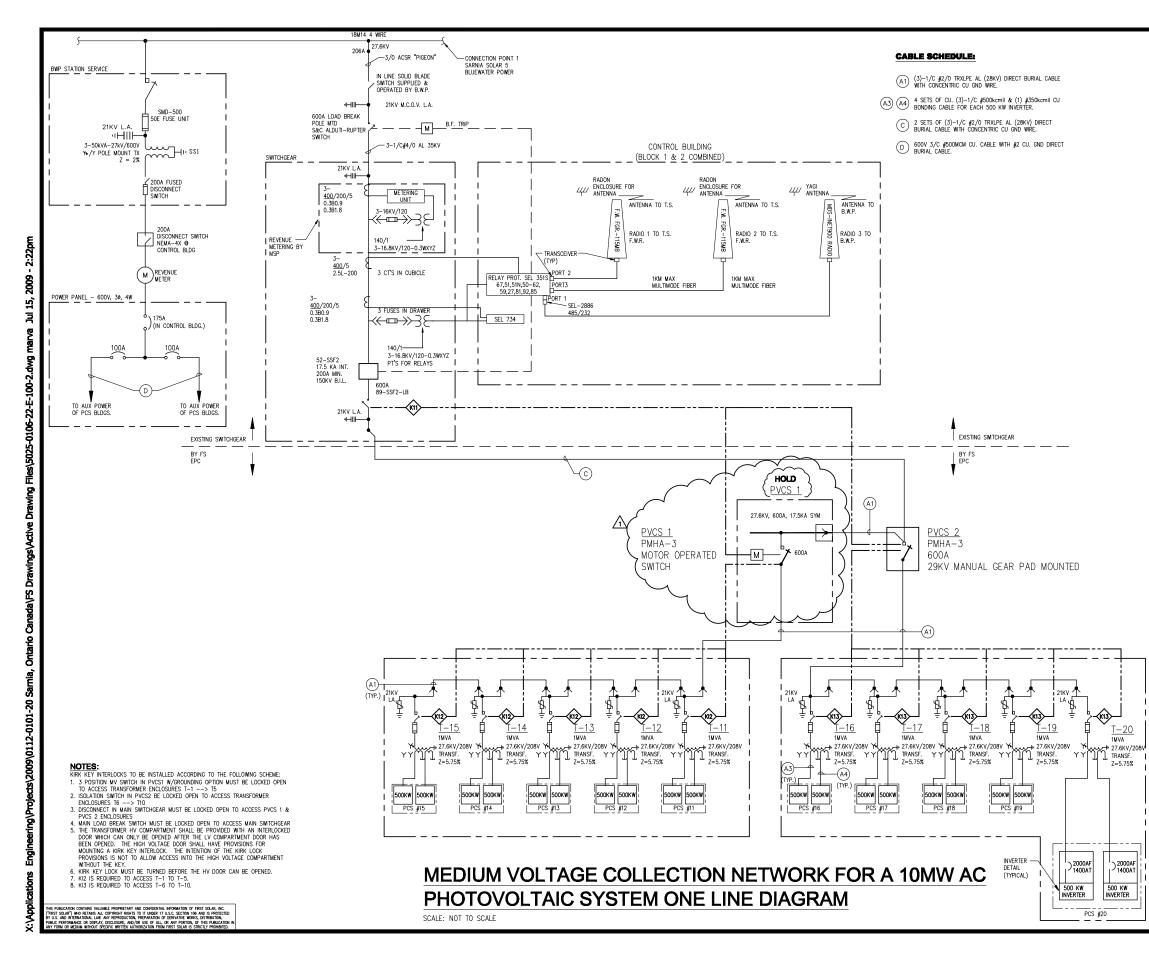
APPENDIX C System Operation Diagram

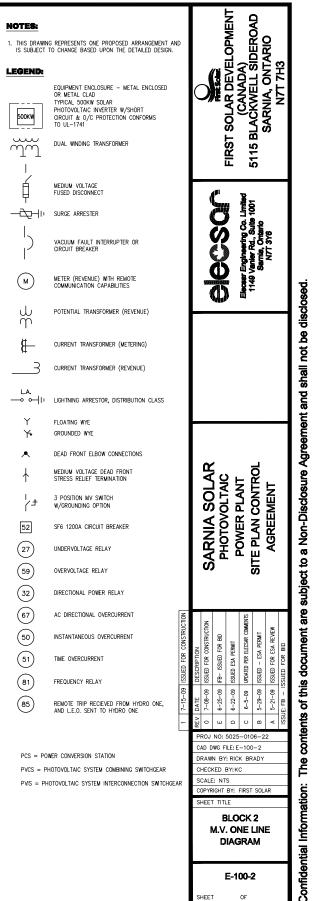






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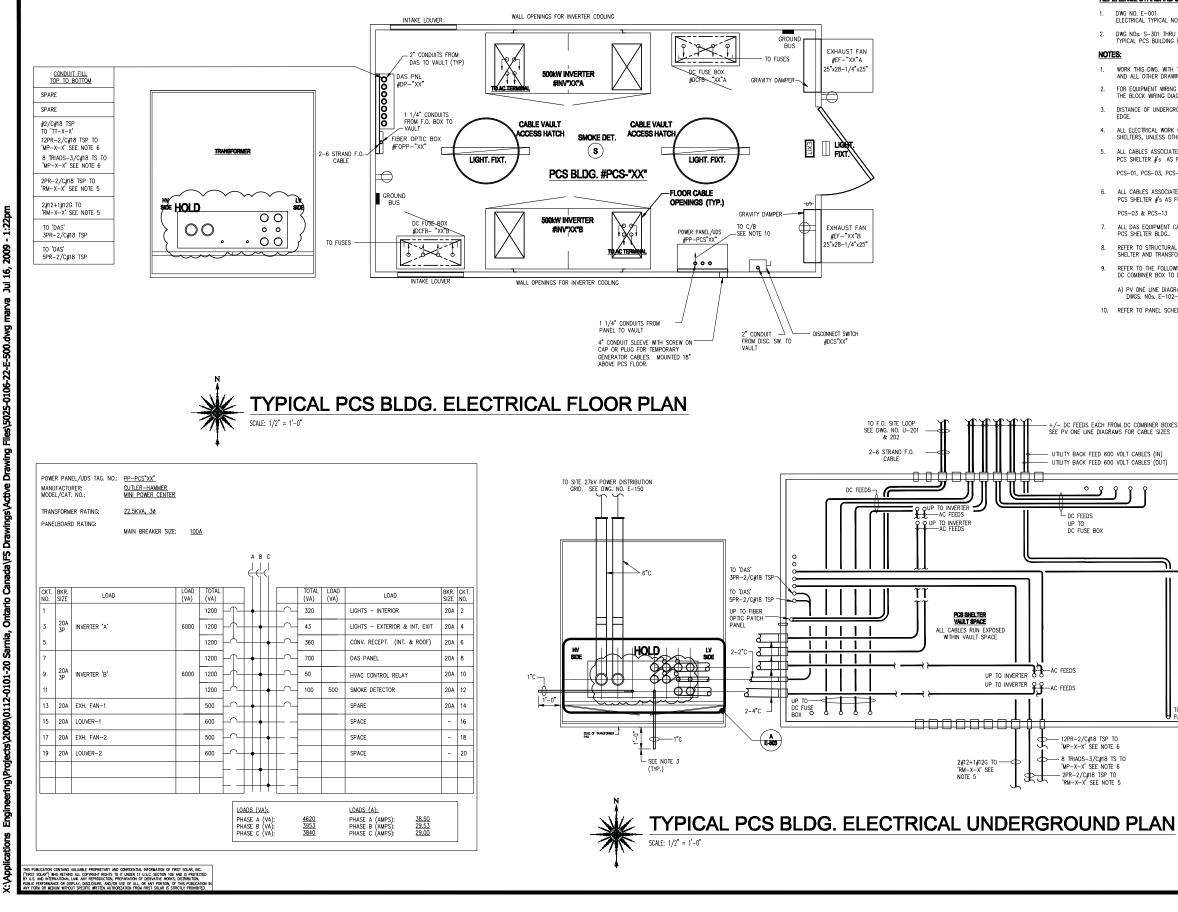
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APPENDIX D

Concrete Enclosure Details





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REFERENCE STANDARD SPECIFICATION:

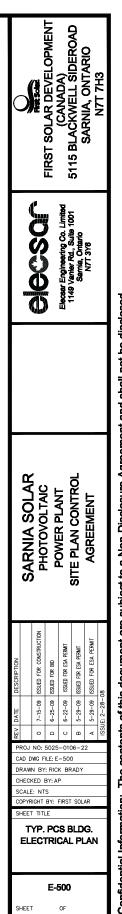
- DWG NO. E-001 ELECTRICAL TYPICAL NOTES, SYMBOLS & ABBREVIATIONS 2.
- DWG NOs. S-301 THRU S-304 TYPICAL PCS BUILDING PLANS AND DETAILS

NOTES:

- WORK THIS DWG. WITH THE STANDARD SPECIFICATION SS-17000 AND ALL OTHER DRAWINGS LISTED UNDER ATTACHMENTS.
- FOR EQUIPMENT WIRING AND INTERCONNECTION DIAGRAM, SEE THE BLOCK WIRING DIAGRAM ON DWG NO. E-710. 2. 3. DISTANCE OF UNDERGROUND CONDUIT TO EXTEND BEYOND PAD EDGE.
- ALL ELECTRICAL WORK ON THIS DWG IS TYPICAL FOR ALL PCS SHELTERS, UNLESS OTHERWISE NOTED.
- 5. ALL CABLES ASSOCIATED WITH 'RM-X-X' IS ONLY TYPICAL FOR PCS SHELTER #'s AS FOLLOWS:
- PCS-01, PCS-03, PCS-05, PCS-11, PCS-13 AND PCS-15,
- 6. ALL CABLES ASSOCIATED WITH 'MP-X-X' IS ONLY TYPICAL FOR PCS SHELTER #'s AS FOLLOWS: PCS-03 & PCS-13
- ALL DAS EQUIPMENT CABLES ARE ENTERING VIA CONDUITS TO PCS SHELTER BLDG.
- 8. REFER TO STRUCTURAL DWGS. FOR EXACT LOCATION OF PCS SHELTER AND TRANSFORMER.
- REFER TO THE FOLLOWING DRAWINGS FOR THE DC CABLING FROM DC COMBINER BOX TO DC FUSE BOX: A) PV ONE LINE DIAGRAMS DWGS. NOs. E-102-1 & E-102-2.
- 10. REFER TO PANEL SCHEDULE IN THIS DWG. FOR CIRCUITS:

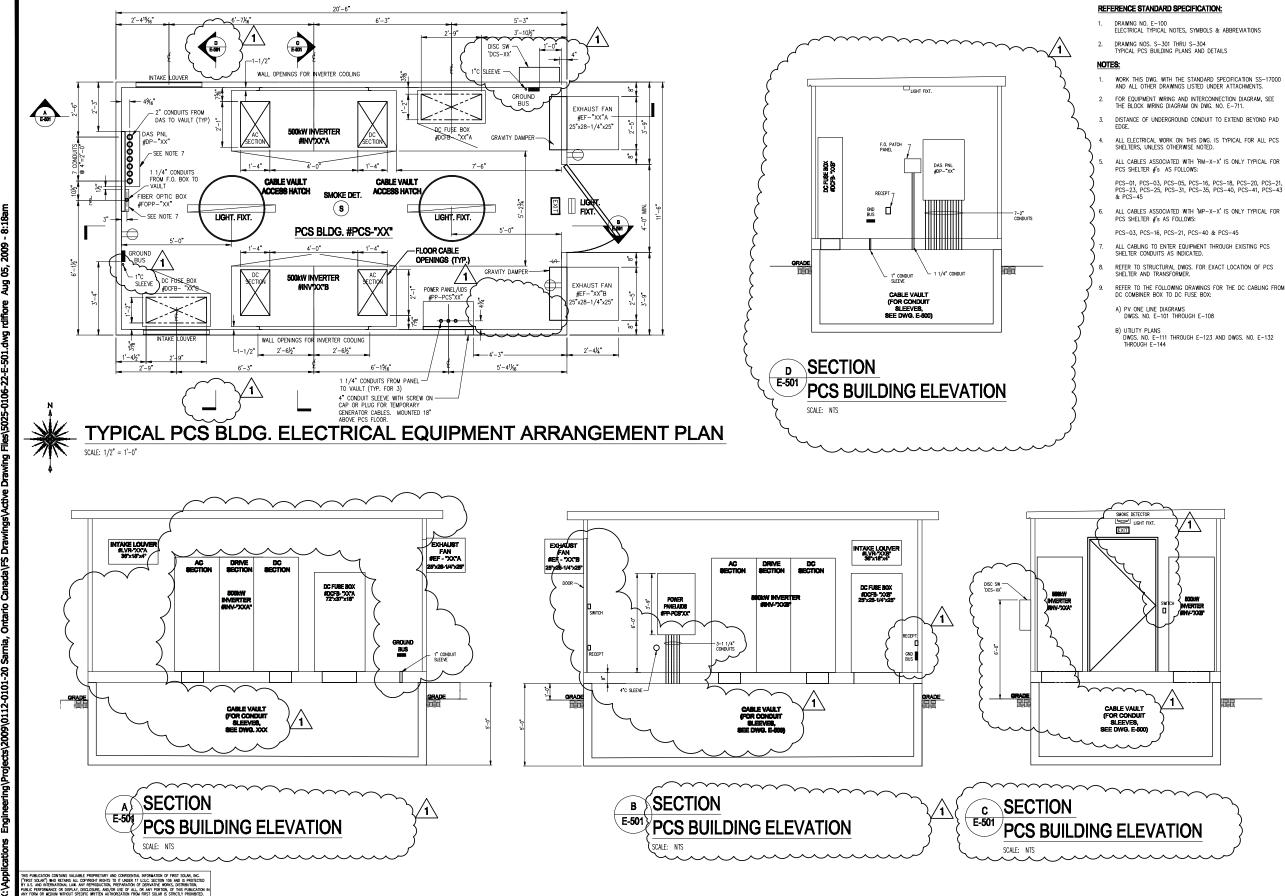
+/- DC FEEDS EACH FROM DC COMBINER BOXES SEE PV ONE LINE DIAGRAMS FOR CABLE SIZES

<u>_____</u>j 1000000000 #2/C#18 TSP TO POWER PANEL DISC. SW.

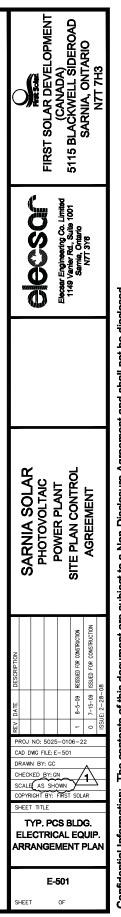


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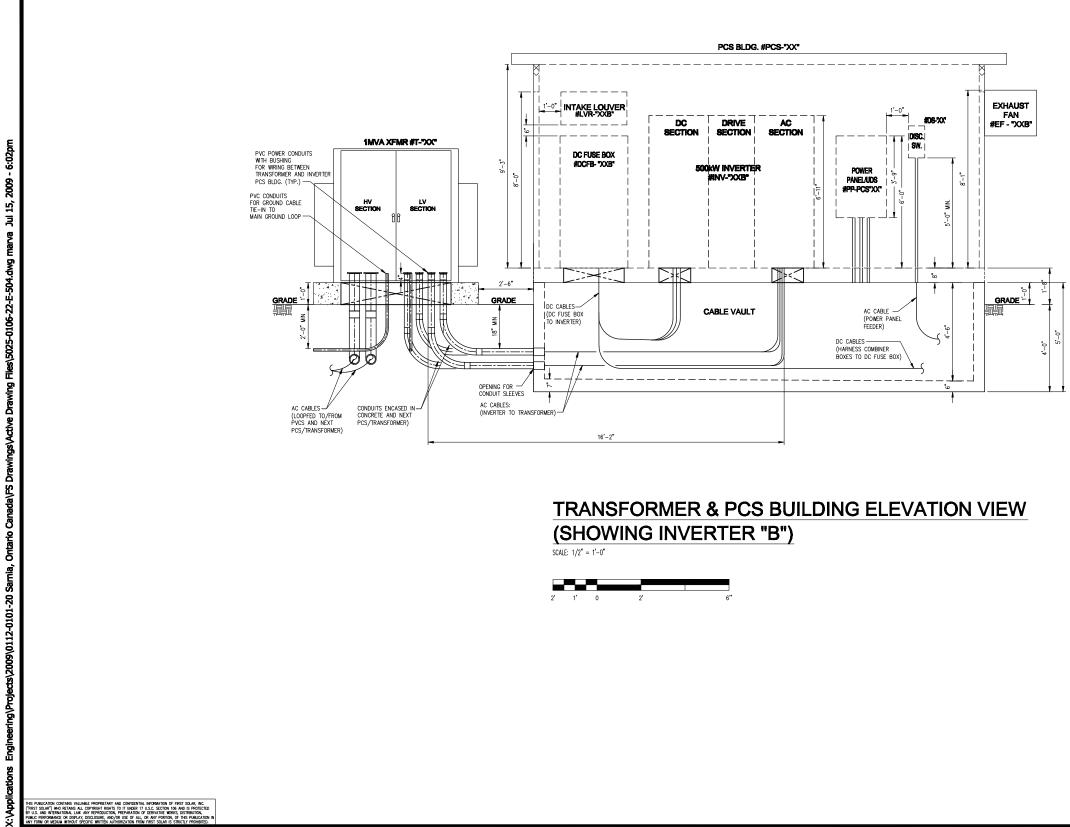


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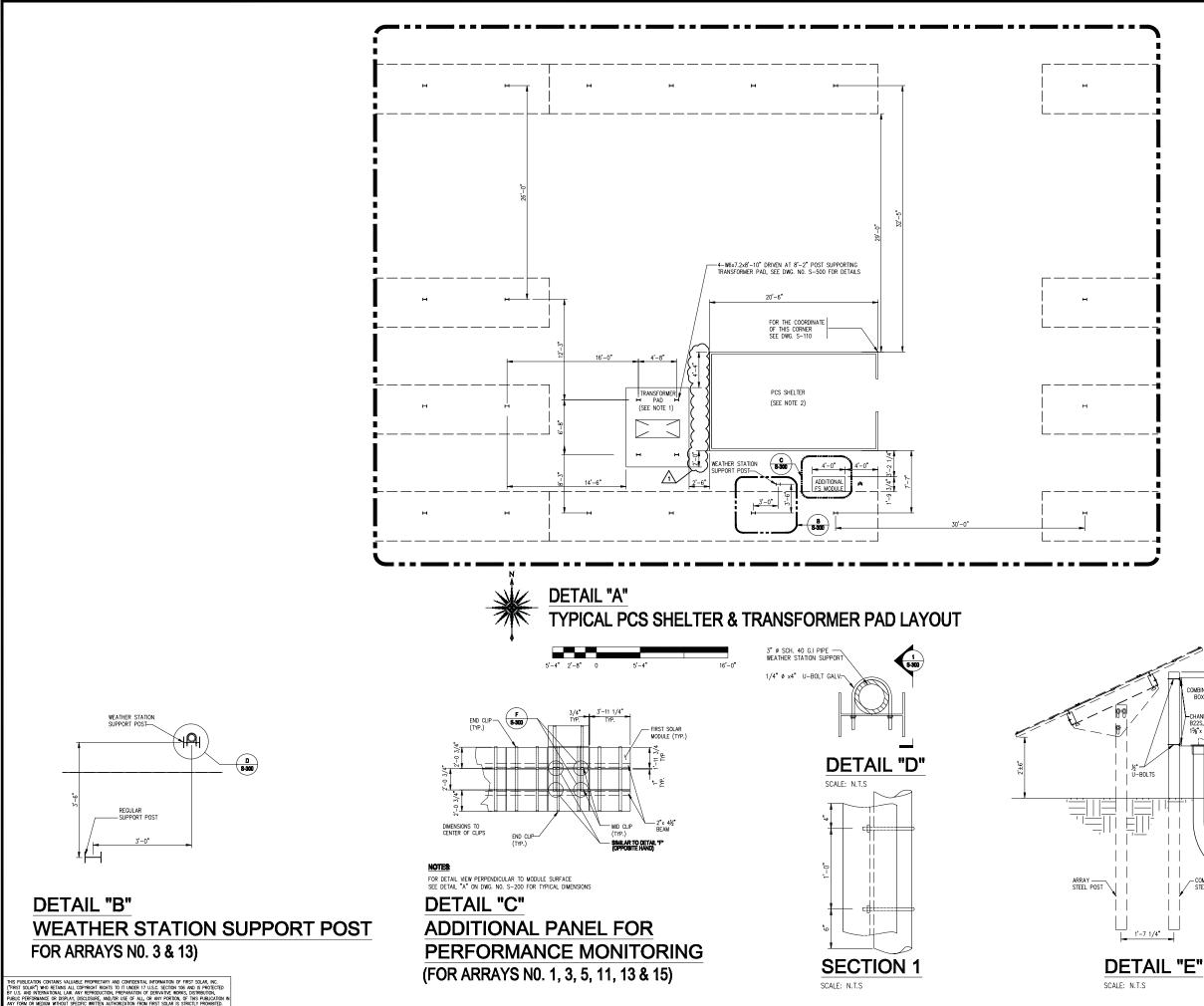


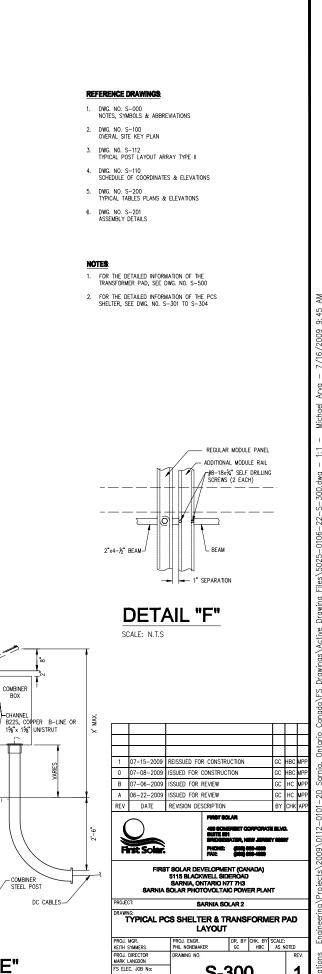
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REFERENCE STANDARD SPECIFICATION:

- 1. DWG NO. E-001 ELECTRICAL TYPICAL NOTES, SYMBOLS & ABBREVIATIONS
- DWG NOs. S-301 THRU S-304 TYPICAL PCS BUILDING PLANS AND DETAILS
- DWG NO. E-503 TYP. PCS BLDG. ELECTRICAL EQUIP. ARRANGEMENT PLAN

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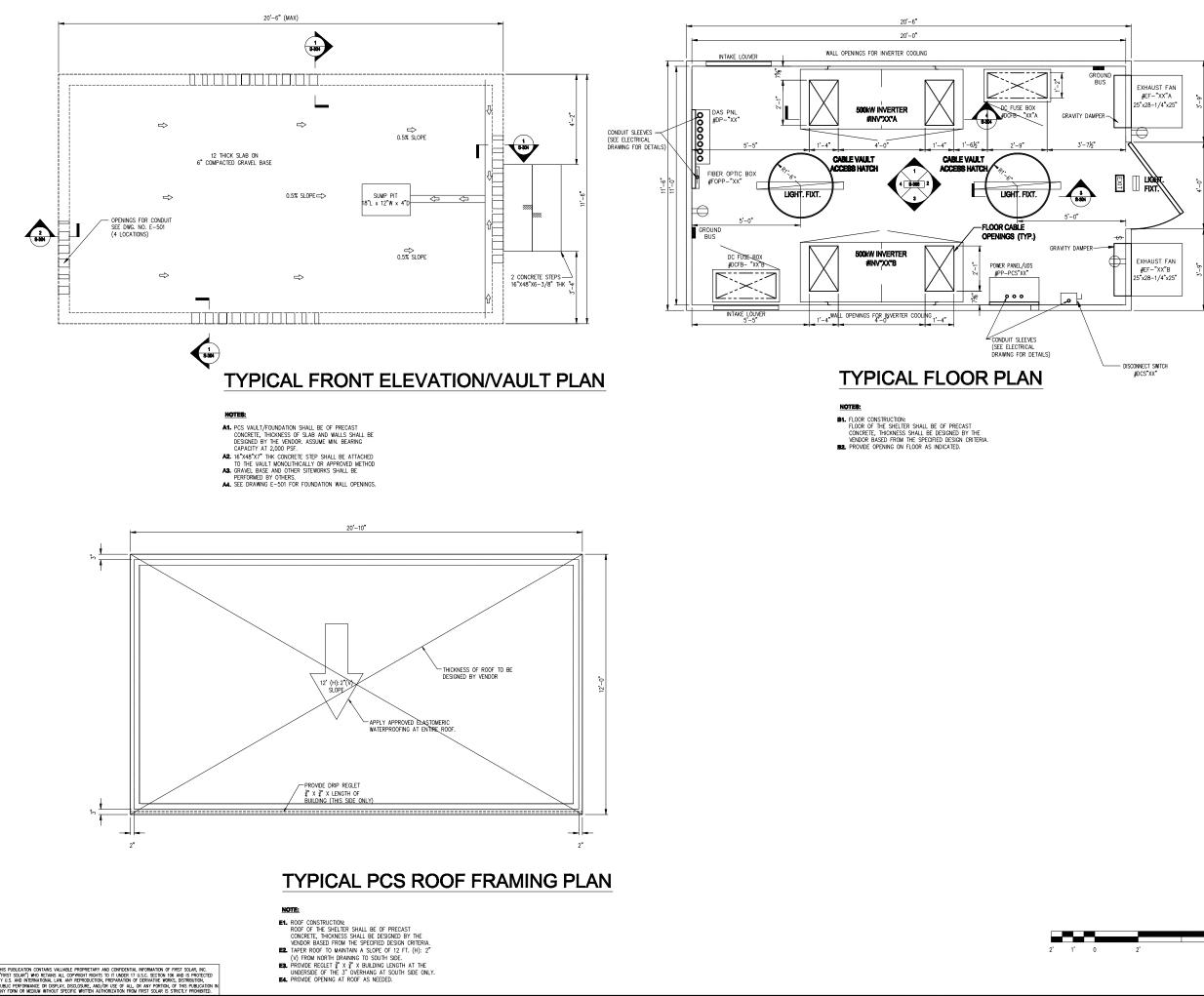


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REFERENCE NOTES :

DWG NO. E-501 PCS ELECTRICAL EQUIPMENT PLAN.

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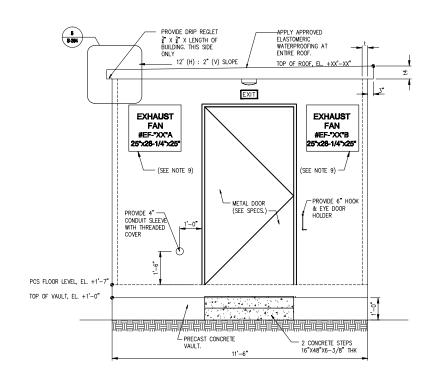
- 1. WORK THIS DWG. WITH THE STANDARD SPECIFICATION.
- 2. VENDOR TO COORDINATE OPENING LOCATIONS WITH ELECTRICAL DRAWINGS
- & VAULT EXTERIOR MEASUREMENTS SHALL MATCH WITH PCS BUILDING EXTERIOR MEASUREMENTS.
- C.S. GUILDING EALERIUM MEASUREMENTS.
 4. VEDIOR STALL PRE-TI/PRE-ASSEMBLE VAULT AND PCS SHELTER AND PROVIDE MATCH MARKINGS TO ASSURE PERFECT ALIGNMENT OF VAULT AND PCS SHELTER ONCE DELIVERED AND ERECTED AT THE JOBSITE.
- JOBSITE. SVENDOR SHALL BE RESPONSIBLE FOR THE LOADING, TRUCKING TO THE JOBSITE, AND COORDINATION WITH THE OWNER DURING THE DEUVERY OF VAULTS AND PCS SHELTER TO THE JOBSITE. COWNER SHALL BE RESPONSIBLE FOR THE SUPPLY OF LIFTING COUPMENT, LABOR AND MISCELLANEOUS TOOLS AND MATERIALS DURING THE UNICADING AND ERECTION OF THE VAULTS AND PCS SHELTER. LIFTING COUPMENT, LABOR SHELTER DURING AND RECTON
- 7. VENDOR SHALL BE RESPONSIBLE FOR THE FOLLOWING EQUIPMENT AND ACCESSORIES AFTER THE ERECTION OF THE VAULTS AND PCS SHELTER BY THE OWNER, AS
- FOLLOWS: A. INSTALLATION OF SEISMIC/CONNECTING PLATES FOR
- A. INSTALLATION OF SEISMIC/CONNECTING PLATES FOR VAULTS AND SHELTER.
 B. ENGINEER/DESIGN, SUPPLY AND ERECT HVAC UNITS INCLUDING ELECTRICAL HOOK-UPS.
- C. ENGINEER/DESIGN, SUPPLY AND INSTALLATION OF AIR TERMINALS. D. SUPPLY AND INSTALL PATCHING AT DEPRESSIONS
- FOR ALL LIFTING LUG LOCATIONS IN ANY PART OF THE VAULT OR PCS SHELTER AND APPLY FINAL COATINGS OR FINISH SURFACE WITH MATERIAL
- CUATINGS OR FINISH SURFACE WITH MATERIAL SMILAR TO THE ADJACENT AREA. E. SUPPLY AND APPLY SEALANT/MASTIC/CAULKS AT ALL POSSIBLE ENTRY POINTS OF WATER INCLUDING BUT NOT LIMITED TO THE JOINTS BETWEEN THE VAULTS AND THE PCS SHELTER, ATTACHMENT OF EXTERNAL EQUIPMENT AND ACCESSORIES, ETC.

STRUCTURAL DESIGN CRITERIA :

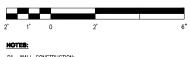
CODE EDITIONS USED - OBC 2006, CAN/CSA-S16-01, CAN/CSA-S136-01 OCCUPANCY GROUP - S-2 OCCUPANCY CATEGORY III TYPE CONSTRUCTION - VB LAND USE ZONE - RENEWABLE ENERGY SQUARE FOOTAGE/ALLOWABLE AREA - 224.25 SF HEIGHT - 11'-6" (APPROX.) ABOVE GRADE OCCUPANT LOAD (PCS) - 1 FLOOR LIVE LOAD - 150 PSF (7.18 kPa) MAXIMUM FLOOR EQUIPMENT LOAD - 6,000 LBS WIND REFERENCE PRESSURES - q50 = 11.5 PSF (0.55 kPa) MAXIMUM |w = 1.25 NET SPECIFIED WIND LOAD - P = 11.8 kN ACTING PERPENDICULAR TO LONG WALL P = 9.7 kN ACTING PERPENDICULAR TO SHORT WALL GROUND SNOW LOADS - 39.2 PSF (1.875 kPa) MAXIMUM BASED ON - Ss = 1.1 kPa, Sr = 0.4 kPa, Is = 1.25 ROOF LIVE LOAD (REDUCEABLE) - 20 PSF SEISMIC DESIGN CRITERIA SITE CLASSIFICATION "C" Ta = 0.2 s IN EACH DIRECTION Fa = 1.0; Fv = 1.0FOR ONTARIO: Sa(0.2) = 0.36, Sa(0.5) = 0.18, Sa(1.0) = 0.063, Sa(2.0) = 0.02S(T) = 0.36le = 1.5, Mv = 1.0, Rd = 2.0, Ro = 1.3 CONCRETE: F'C = 5,000 PSI @ 28 DAYS REINFORCING STEEL: ASTM A-615, GRADE 60 WIRE MESH: ASTM A-496 OR A-497 7-15-2009 ISSUED FOR CONSTRUCTION C KDK C KDK T B 06-04-2009 UPDATED DRAWING NUMBER A 05-19-2009 ISSUED FOR PROPOSAL REV DATE REVISION DESCRIPTION FINET BOLAR HEI SCHEFTER Buite oct First Solar. . NEW JER FIRST SOLAR DEVELOPMENT (CANADA) 5115 BLACKWELL SIDERDAD SARNIA, ONTARIO N77 7H3 SARNIA SOLAR PHOTOVOLTAIC POWER PLANT SARNIA SOLAR 2 PCS SHELTER FLOOR AND VAULT PLANS DR. BY CHK. BY SCALE: G.C KDK 1/2"=1'-0" NONEMAKER KEITH SYMMERS PROJ. DIRECTOR MARK LANGDON FS ELEC. JOB No: S-301 0 5025-0108-22 THIS PRINT IS NOT TO BE USED FOR CONSTRUCTION UNLESS NOTE AND SIGNED OK FOR CONSTRUCTION ABOVE LAST REVISIOI



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TYPICAL FRONT ELEVATION

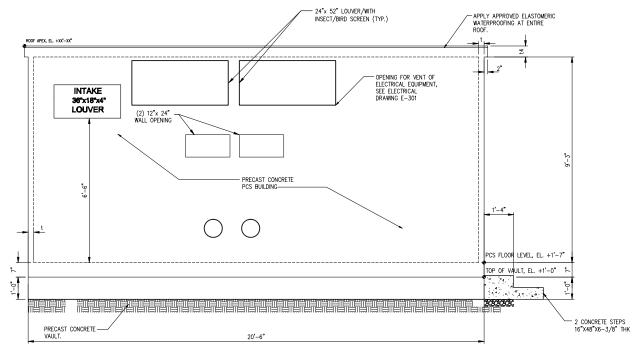


D1. WALL CONSTRUCTION: WALL OF THE SHELTER SHALL BE OF PRECAST CONCRETE, THICKNESS SHALL BE DESIGNED BY THE VENDOR BASED FROM THE SPECIFIED DESIGN CRITERIA.

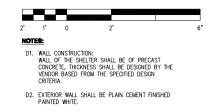
D2. EXTERIOR WALL SHALL BE PLAIN CEMENT FINISHED PAINTED WHITE.

D3. PROVIDE OPENING ON WALLS AS INDICATED.

D4. PROVIDE SEALANT AT ALL JOINTS/CONECTIONS.



TYPICAL LEFT ELEVATION



D3. PROVIDE OPENING ON WALLS AS INDICATED.

D4. PROVIDE SEALANT AT ALL JOINTS/CONECTIONS.

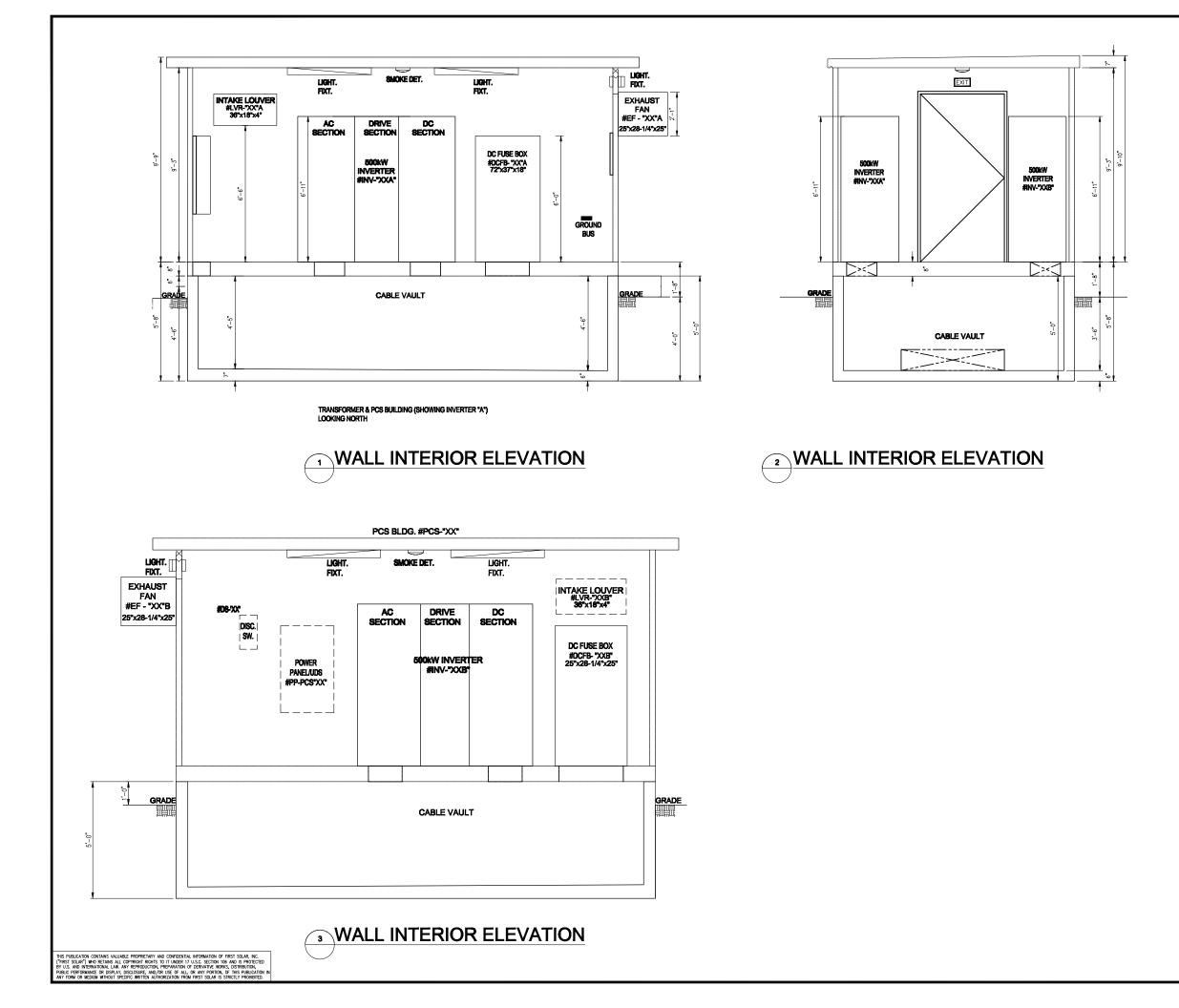
NOTES:

1. SEE DWG S-301 FOR ADDITIONAL NOTES.





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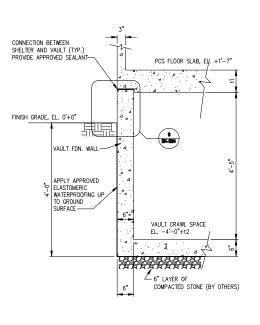


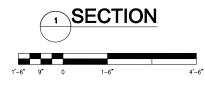
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0 07-15-2009) ISSUED FOR CONSTRU	CTION		PTR	KDK	ΤZ
B 06-04-200					KDK	
A 05-19-200						
		-		-	KDK	
REV DATE	REVISION DESCRIPT	TON		BY	CHK	APP
First Sola			EW .00700 00-4000 00-4000		-	
	ST SOLAR DEVELO 5115 BLACKWELL SARNIA, ONTARI SOLAR PHOTOVO	. SIDERÒAD O N7T 7H3) -	п		
DRAWING:	GARINA	A OULAR Z				_
	HELTER INTER	IOR ELE	VATIO	NS		
proj. Mgr. Keith symmers	PROJ. ENGR. Phil Nonemaker	DR. BY G.C	CHK. BY KDK	SCALE	'-0 *	
PROJ. DIRECTOR MARK LANGDON	DRAWING NO.				R	EV.
FS ELEC. JOB No:	∣ ເ	-303	2		1	ן נ
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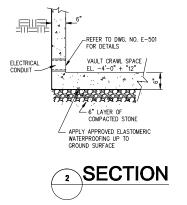


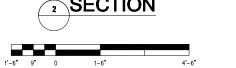
NOTES:

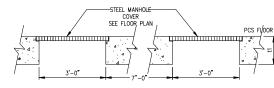
SEE DWG SS-17000-SK-S01 FOR ADDITIONAL NOTES.

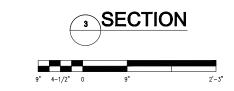


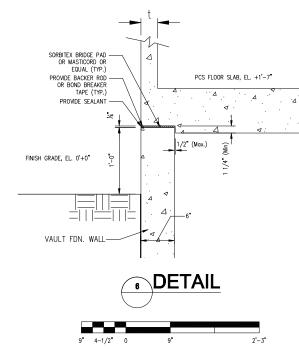


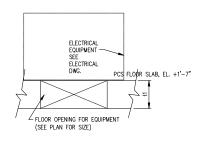


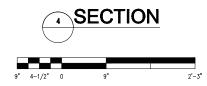


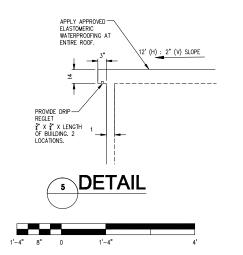












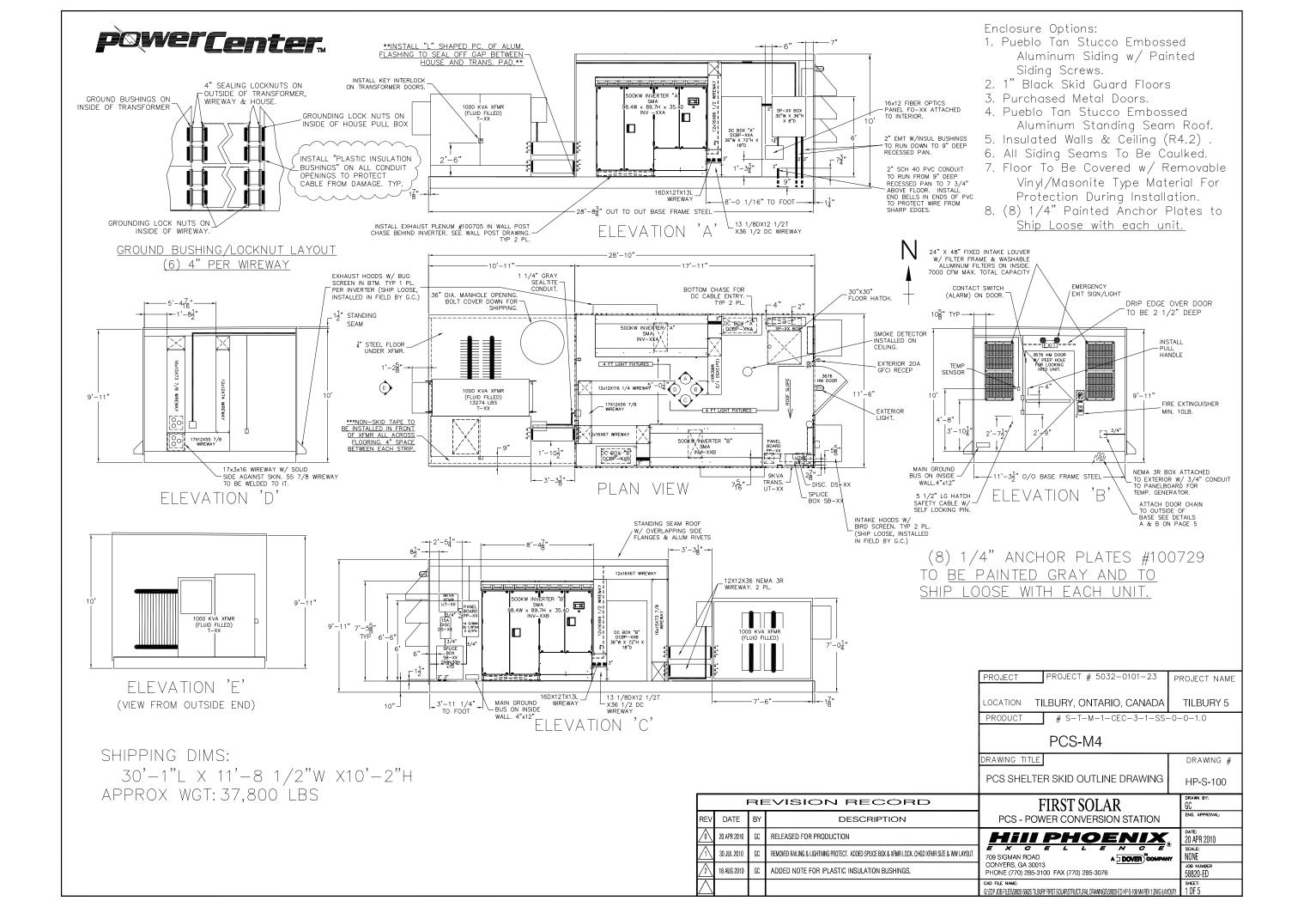
NOTES:

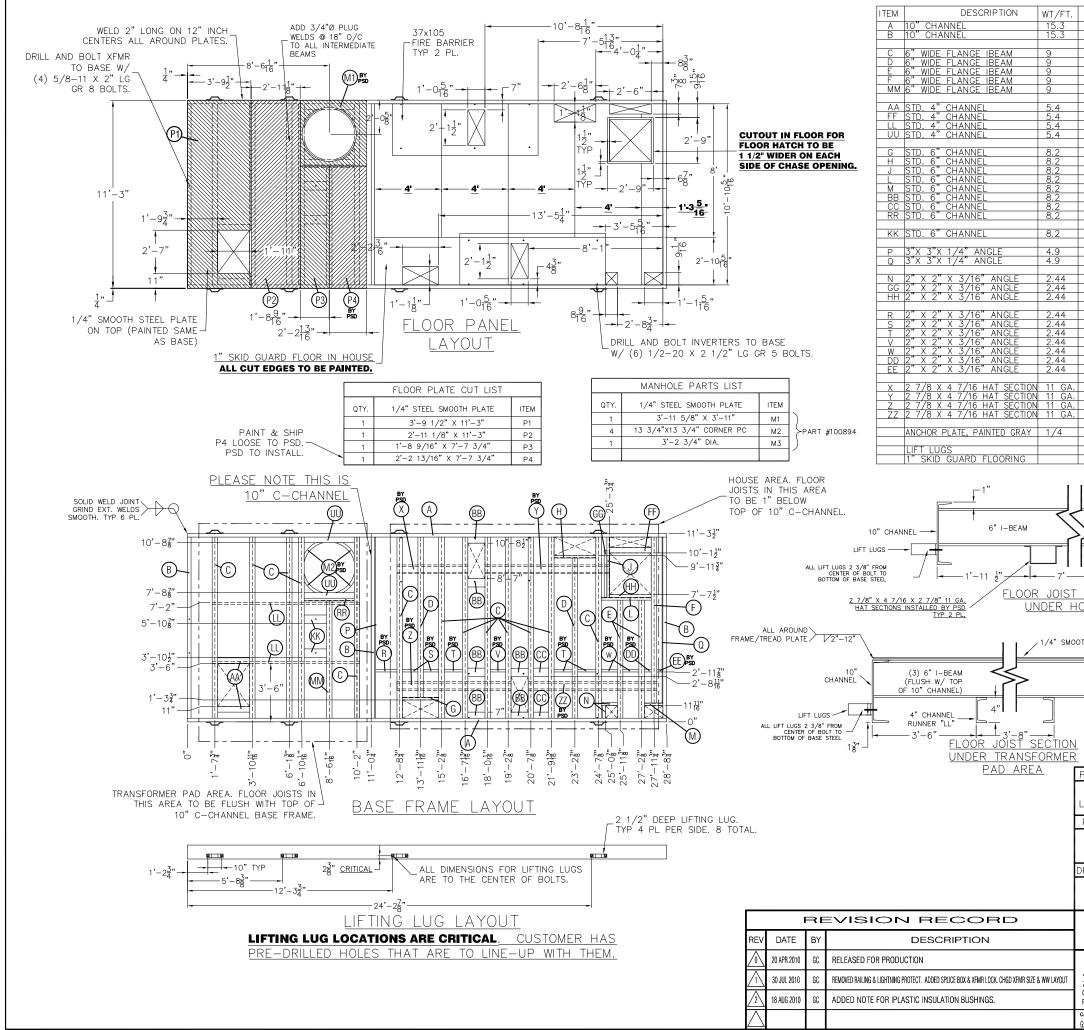
1. SEE DWG S-301 FOR ADDITIONAL NOTES.

PCS FLOOR SLAB, EL. +1'-7"

0	07-15-2009	ISSUED FOR CONSTRUC	CTION		G.C	KDK	TZ
в	06-04-2009	UPDATED DRAWING NU	MBER			KDK	TZ
Α	05-19-2009	ISSUED FOR PROPOSAL	_		G.C	KDK	ΤZ
REV	DATE	REVISION DESCRIPT	ION		BY	СНК	APP
F	rst Solar.	<u>eur</u>					
- NFI	FIRS		E CON CREMATER, M (1990) 4 (1990) 4 (19	IADA)	EYGON		
PROJEC	FIR\$ SARNIA	T SOLAR DEVELOP 5115 BLACKWELL SARNIA, ONTARIO SOLAR PHOTOVOL	E CON CREMATER, M (1990) 4 (1990) 4 (19	IADA)	EYGON		
PROJEC	FIRS SARNIA DT: 16:	T SOLAR DEVELOP 5115 BLACKWELL SARNIA, ONTARIO SOLAR PHOTOVOL	MENT (CAN SIDEROAD O N7T 7H3 TAIC POWI SOLAR 2	ew Jerne 100-4000 1400A) ER PLAN	EY 6600		
PROJ.	FIR8 SARNIA CT: 46: PCS SH	T SOLAR DEVELOP S115 BLACKWELL SARNIA SARNIA SARNIA SARNIA	MENT (CAN SIDEROAD N7T 7H3 TAIC POWI SOLAR 2	ew Jerne 100-4000 1400A) ER PLAN	ет они чт ONS		
PRAWIN PROJ. EETTH S PROJ.	FIRS SARNIA CT: PCS SH MGR.	T SOLAR DEVELOP 5115 BLACKWELL BARNIA, ONTARK SOLAR PHOTOVOL SARNIA ELTER DETAIL	MENT (CAN SIDEROAD DIVIT 713 TAIC POWI SOLAR 2 .S AND S		NT ONS SCALE:	TED	EV.
PROJ. KEITH S PROJ. MARK L	FIRS SARNIA CT: IG: PCS SH MGR. SYMMERS DIRECTOR	T SOLAR DEVELOP S115 BLACKNELL SARNIA, ONTARI SOLAR PHOTOVOL SARNIA ELTER DETAIL PROJ. ENGR. PROJ. ENGR. PROJ. ENGR. PROJ. ENGR. DRAWING NO.	MENT (CAN SIDEROAD DIVIT 713 TAIC POWI SOLAR 2 .S AND S		NT ONS SCALE:	TED R	ev.)

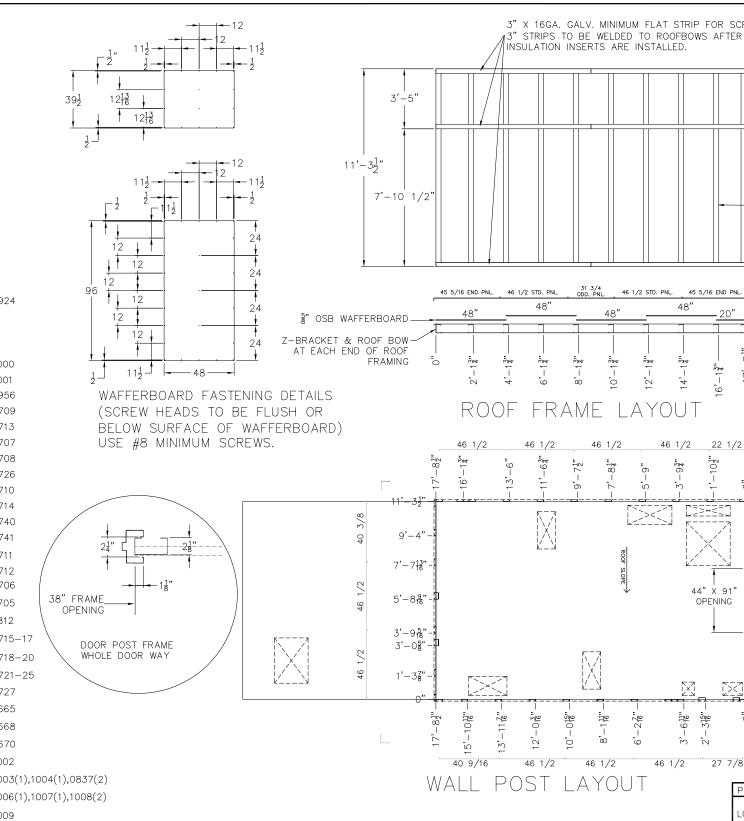
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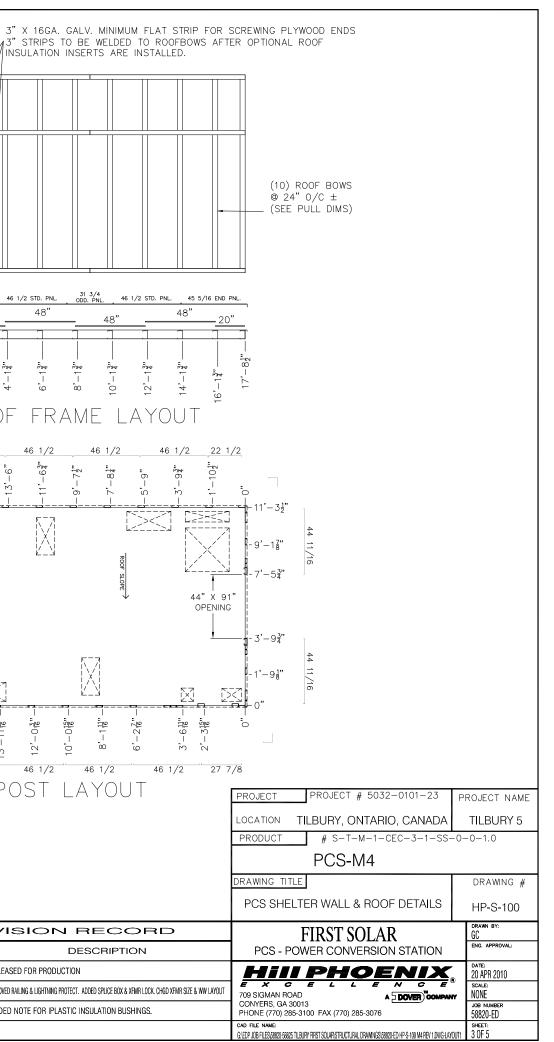


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-	PROJE	ст	PROJE	CT # 503	2-0101-23	PROJECT NAME
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F	PRODU				CEC-3-1-SS-	
			PC	S-M4		
	RAWIN	G TI				DRAWING #
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			FIRS	FSOLA	R	drawn by: GC eng. approval:
╞	PC	:S - F			IN STATION	. DATE:
$\left \right $						© 20 APR 2010 scale: NONE
	709 SIGI				A DOVER COMPAN	
1	CONYEF PHONE	(770) 2	30013 85-3100 FAX (7	70) 285-3076		JOB NUMBER 58820-ED

DESCRIPTION	QTY.	LENGTH	
6" X 14 GA. Z-BRACKET	4	106 1/4	
6" X 14 GA END Z-BRACKET	2	135 3/8	
6" Z-BRACKET SPLICE PLATE	2	10	
3 1/2" X 5 1/8" 16GA C-ROOF BOW	10	135 1/4	
3" X 16 GA STRIPS	3	120	
3" X 16 GA STRIPS	3	92 1/4	
4 1/2" WALL POST X 14 GA	11	112 7/8	
4 1/2" WALL POST X 14 GA	2	50 1/2"	
4 1/2" WALL POST X 14 GA	2	99 5/16"	
4 1/2" WALL POST X 14 GA	2	98 5/16"	
4 1/2" WALL POST X 14 GA	12	111 7/8	
4 1/2" WALL POST X 14 GA	4	24 1/4	
4 1/2" WALL POST X 14 GA 4 1/2" WALL POST X 14 GA	1	8 1/4	
2 1/8" X 4 1/2" WALL POST X 14 GA	21	46 3/8	1.00
4 1/2" WALL POST X 14 GA	 2	13 5/8 112 1/2	100
4 1/2" WALL POST X 14 GA	1	8 7/8	
	1		
3" X 4 1/2" WALL POST X 14 GA	1	112 1/8	101
3" X 4 1/2" WALL POST X 14 GA	1	112 5/16	101
2 3/8" x 4 1/2" WALL POST X 14 GA	2	111 7/8	100
7 3/16" WALL POST X 14 GA	1	111 7/8	100
7 3/16" WALL POST X 14 GA	1	112 5/8	100
4" WALL POST X 14 GA	1	99 5/16"	100
4" WALL POST X 14 GA	1	98 5/16"	100
3" WALL POST X 14 GA	2	50 1/2"	100
2 7/8" WALL POST X 14 GA	1	111 7/8	100
2 7/8" WALL POST X 14 GA	1	112 7/16	100
3 1/2" WALL POST X 14 GA	1	111 7/8	100
3 1/2" WALL POST X 14 GA	1	112 7/16	100
4 1/2" X 2 1/8" DOOR POST	1	112 1/16	100
4 1/2" X 2 1/8" DOOR POST 4 1/2"X2 1/8" DOOR HEADER-14 GA	<u>1</u> 1	112 7/16 44"	100 100
EXHAUST PLENUMS, INVERTER BTM REAR-14 GA	2		
	1	5 7/8 X 50 7/16	100
PAN, SP-1 & FIBER OPTIC CHASE FILLER		26 15/16X49 6/16	100
20 X 32 7/8 RAIN HOOD TOP W/BIRD SCREEN	2	32 7/8	100
20 X 32 7/8 RAIN HOOD BTM W/BIRD SCREEN	4	32 7/8	100
12 X 57 1/2 RAIN HOOD W/BUG SCREEN	2	57 1/2	100
FILTER FRAME PANEL, 14 GA.	2	24 1/16 X 51 1/4	100
Z-BRKT, FILTER FRAME, 14 GA.	4	23 3/8	100
HAT-SHAPED BRKT, FILTER FRAME, 14 GA.	2	23 13/16	100
FILTER END COVER, 14 GA.	2	50 1/2	100
17X3X16 WIREWAY W/(3) CUTOUTS	1	17X3X16	101
17X12X55 7/8 WIREWAY W/CUTOUT	1	55 7/8	101
16X15X73 7/8 WIREWAY W/(3) CO	1	73 7/8	101
SUPPORT, EXT. WIREWAY	1	36X31 7/16	101
		, ,	
STD 1" WALL & ROOF INSULATION W/SOLID L	INERS	1	
PUEBLO TAN EMBOSSED ALUM. WALL & ROOF			
STD. 5/8" OSB WAFFERBOARD ROOF UNDERL			
,			



	I	RE	EVISION RECORD
REV	DATE	BY	DESCRIPTION
\triangle	20 APR 2010	GC	RELEASED FOR PRODUCTION
1	30 JUL 2010 GC REMOVED		REMOVED RAILING & LIGHTNING PROTECT. ADDED SPLICE BOX & XFMR LOCK. CHGD XFMR SIZE & WW LAYOUT
2	18 AUG 2010	GC	ADDED NOTE FOR IPLASTIC INSULATION BUSHINGS.
\wedge			



48"

 $14' - 1\frac{3}{4}''$

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3'-6<u>11</u>" -2'-3<u>15</u>" -

46 1/2

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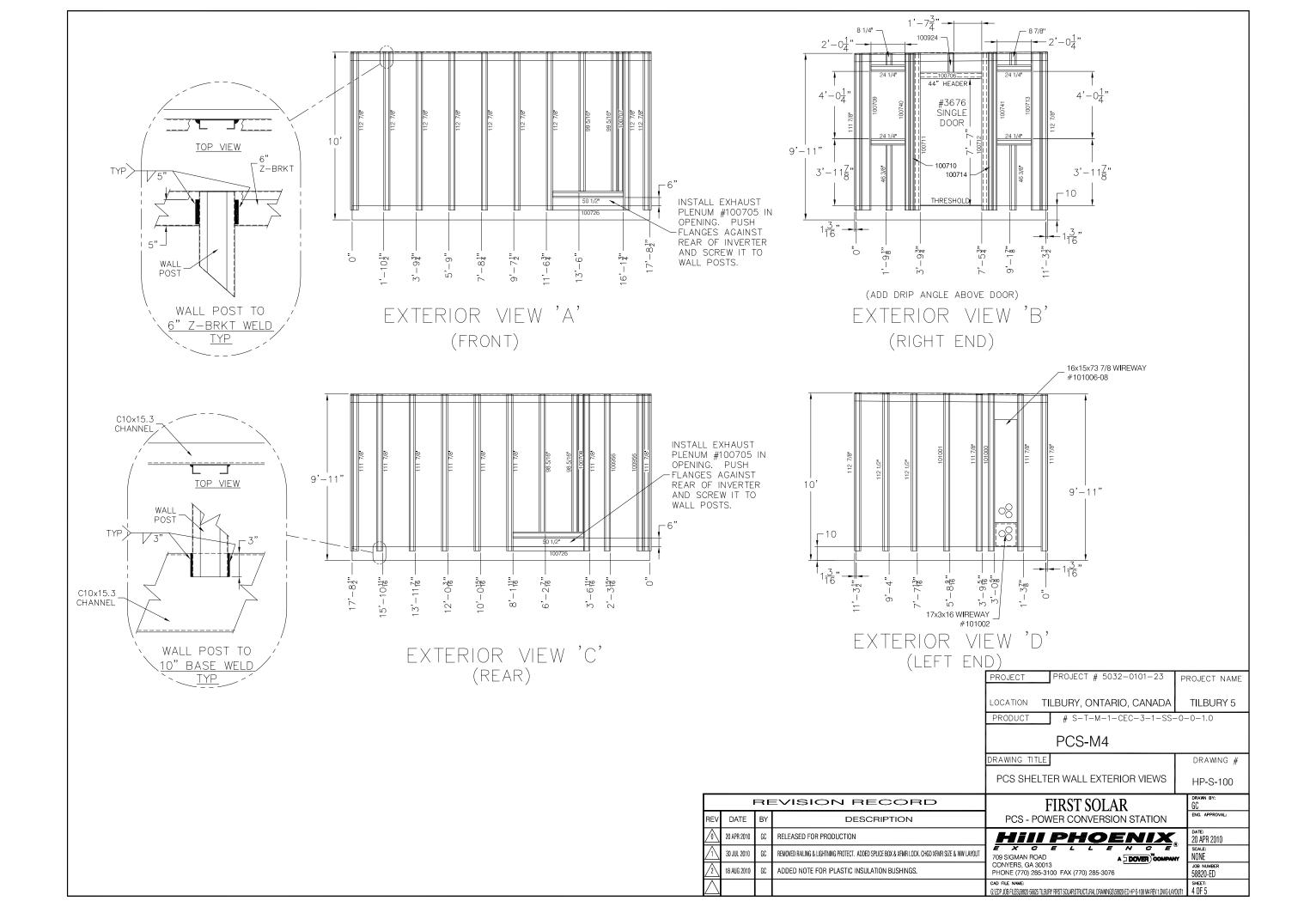
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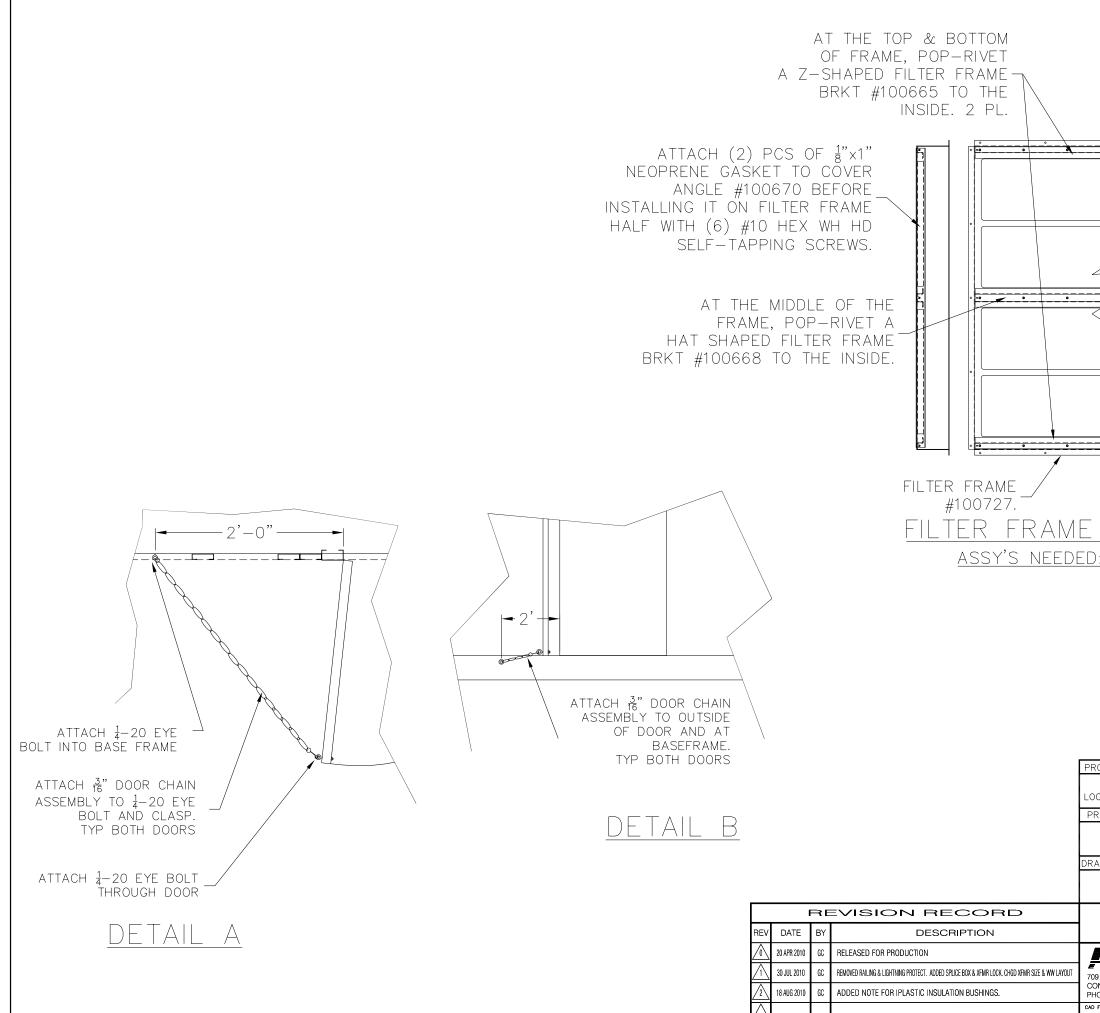
12'-13"

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2<u>76</u>"

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ATTACH (2) PCS NEOPRENE GASK INSIDE WALL OF FILTER FRAME H 2 PL. E ASSY ED: 2	ET TO The
PROJECT PROJECT # 5032-0101-23	PROJECT NAME
LOCATION TILBURY, ONTARIO, CANADA	TILBURY 5
PRODUCT # S-T-M-1-CEC-3-1-SS-	-0-0-1.0
PCS-M4	
DRAWING TITLE PCS SHELTER FILTER	DRAWING #
FRAME ASSEMBLY	HP-S-100 drawn by:
FIRST SOLAR PCS - POWER CONVERSION STATION	GC eng. approval:
HIII PHOENIX	DATE: 20 APR 2010
709 SIGMAN ROAD A DOVER, GA 30013	SCALE: NONE JOB NUMBER
PHONE (770) 285-3100 FAX (770) 285-3076 cad file name:	58820-ED Sheet:
G/EDP JOB FILESIS8820-58825 TILBURY FIRST SOLARISTRUCTURAL DRAWINGS/58820-ED HP-S-100 MA REV 1.DWG-LAYO	DUT1 5 OF 5







Estimated Source PWL from Measurement data, dB re. $20x10^{-12}$ W



Description	Data Source	31.5	63	125	250	500	1000	2000	4000	8000	dBA
Pauwels 1000 kVA 27600Y/15935 2X 208Y/120 Transformer	Measured (Appendix G)	71	74	72	71	68	64	60	61	57	70
Xantrex Inverter Enclosure	Measured (Appendix G)	84	81	84	85	85	84	80	75	85	89
SMA Inverter	Measured (Appendix G)	80	81	75	79	79	73	75	77	72	83







CERTIFICATE of CALIBRATION

Make :	PCB Piezotronics	Reference # :	88771
Model :	377A60A	Customer :	Golder Associates Ltd Mississauga, ON
Descr. :	Microphone		
Serial # :	: 1022	P. Order :	Stefan

Cal. status : Received in spec's, no adjustment made. Tested with L&D LS3000+ s# 182

JOLA Instruments Inc. certifies that the above listed instrument was calibrated on date noted and was released from this laboratory performing in accordance with the specifications set forth by the manufacturer.

Unless otherwise noted in the calibration report a 4:1 accuracy ratio was maintained for this calibration.

Our calibration system complies with the requirements of ISO-17025 standard, working standards used for calibration are certified by or traceable to the National Research Council of Canada or the National Institute of Standards and Technology.

Calibrated : Jan 06, 2009

Asset # : MS000008

By:

Cal. Due : Jan 06, 2010

J. Raposo

Temperature : 23 °C \pm 2 °C Relative Humidity : 45 % \pm 20 %

Standards used : J-129 J-163 J-216

JOLA Instruments Inc.

REPAIR AND CALIBRATION TRACEABLE TO NRC AND NIST

88 Judge Rd. Toronto, ON, M8Z 5B4 Phone : 416 234 0354

Fax: 416 234 9562

http: // www.jola.com e-Mail: jola @ jola.com

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CERTIFICATE of CALIBRATION

Make :	Larson Davis	Reference # :	88581
Model :	3000+	Customer :	Golder Associates Ltd Mississauga, ON
Descr. :	Analyzer FFT 2ch, SLM type	1	
Serial # :	182	P. Order :	Stefan

Asset # : MS000009

Cal. status : Received in spec's, no adjustment made. With PRM902s#3553 and PCB 377A60 s#1022

JOLA Instruments Inc. certifies that the above listed instrument was calibrated on date noted and was released from this laboratory performing in accordance with the specifications set forth by the manufacturer.

Unless otherwise noted in the calibration report a 4:1 accuracy ratio was maintained for this calibration.

Our calibration system complies with the requirements of ISO-17025 standard, working standards used for calibration are certified by or traceable to the National Research Council of Canada or the National Institute of Standards and Technology.

By:

Calibrated : Jan 05, 2009

Cal. Due : Jan 05, 2010

J. Raposo

Temperature : 23 °C \pm 2 °C Relative Humidity : 45 % \pm 20 %

Standards used : J-203 J-215 J-216

JOLA Instruments Inc.

REPAIR AND CALIBRATION TRACEABLE TO NRC AND NIST88 Judge Rd. Toronto, ON, M8Z 5B4http://www.jola.comPhone : 416 234 0354Fax: 416 234 9562http://www.jola.come-Mail: jola@jola.com

The copyright of this document is the property of JOLA Instruments Inc. Any reproduction other then in full requires written approval!

West Caldwell Calibration Laboratories Inc.

Certificate of Calibration

for

Manufactured By: Model No.: Serial No.: Calibration Recall No.:

CALIBRATOR BRUEL & KJAER 4230 565639 : C6270

Submitted by:

Customer:

Company: Address: Golder Associates Ltd.

The subject instrument was calibrated to the indicated specification using standards traceable to the National Institute of Standards and Technology or to accepted values of natural physical constants. This document certifies that the instrument met the following specification upon its return to the submitter.

West Caldwell Calibration Laboratories Specification No.

4230 B&K (see attached)

Upon receipt for Calibration, the instrument was found to be:

Within (X) see attached Report of Calibration

the tolerance of the indicated specification.

West Caldwell Calibration Laboratories' calibration control system meets the following requirements, ISO 10012-1 MIL-STD- 45662A, ANSI/NCSL, Z540-1, IEC Guide 25, ISO 9001:2000 and ISO/IEC 17025:2005

Note: With this Certificate, Report of Calibration is included.

Calibration Date: 08 March 2007

Certificate No: C6270 -4

QA Doc. #1051 Rev. 2.0 10/1/01

Certificate Page 1 of 1

Approved by:

Stanley Christopher Quality Manager



220 Rutherford Rd. S., Unit 210, Brampton, Ontario L6W 3J6 Canada

ISO 9001:2000 Registered Company Calibration Traceable To N. I. S. T.



Phone: (905) 595-1107

Fax: (905) 595-1108



Certificate of Calibration and Conformance

Certificate Number 2009-120808

Instrument Model 2260, Serial Number 0263, was calibrated on 04AUG2009. The instrument meets factory specifications per Procedure D0001.8089.

New Instrument Date Calibrated: 04AUG2009 Calibration due:

Calibration Standards Used

MANUFACTURER	MODEL	SERIAL NUMBER	INTERVAL	CAL. DUE	TRACEABILITY NO.
Hewlett Packard	34401A	US36015216	12 Months	06MAY2010	4342531
Larson Davis	LDSigGn / 2209	0097 / 0118	12 Months	20JUL2010	2009-120295

Reference Standards are traceable to the National Institute of Standards and Technology (NIST)

Calibration Environmental Conditions

Temperature: 24 ° Centigrade

Relative Humidity: 29 %

Affirmations

This Certificate attests that this instrument has been calibrated under the stated conditions with Measurement and Test Equipment (M&TE) Standards traceable to the U.S. National Institute of Standards and Technology (NIST). All of the Measurement Standards have been calibrated to their manufacturers' specified accuracy / uncertainty. Evidence of traceability and accuracy is on file at Provo Engineering & Manufacturing Center. An acceptable accuracy ratio between the Standard(s) and the item calibrated has been maintained. This instrument meets or exceeds the manufacturer's published specification unless noted.

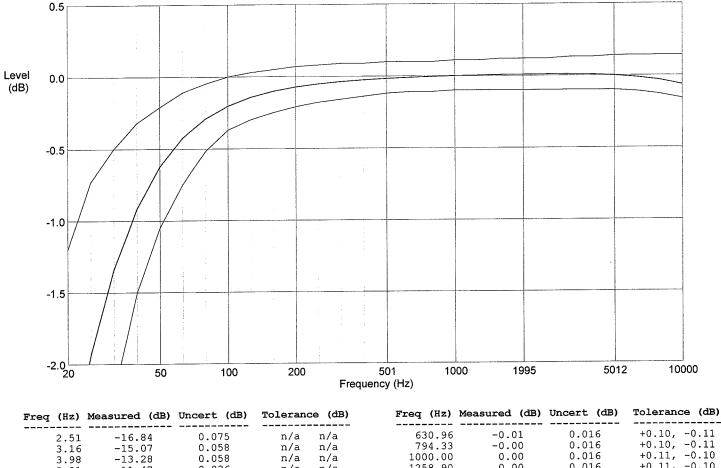
This calibration complies with the requirements of ISO 17025 and ANSI Z540. The collective uncertainty of the Measurement Standard used does not exceed 25% of the applicable tolerance for each characteristic calibrated unless otherwise noted.

The results documented in this certificate relate only to the item(s) calibrated or tested. A one year calibration is recommended, however calibration interval assignment and adjustment are the responsibility of the end user. This certificate may not be reproduced, except in full, without the written approval of the issuer.

Signed:

Preamplifier Model: 2260-Low Serial Number: 0263 Certificate of Electrical Conformance

Frequency response of this model 2260-Low preamplifier was tested at a level of 1 Vrms with 18pF microphone capacitance and driving a short cable. Output level at 1kHz is 0.8914 Vrms (-0.999 dBV), uncertainty 0.033 dB. Results are displayed relative to the level at 1kHz.



2.51	-10.84	0.075	II/a II/a	030.50	0.01	0.010	
3.16	-15.07	0.058	n/a n/a	794.33	-0.00	0.016	+0.10, -0.11
3.98	-13.28	0.058	n/a n/a	1000.00	0.00	0.016	+0.11, -0.10
5.01	-11.47	0.036	n/a n/a	1258.90	0.00	0.016	+0.11, -0.10
6.31	-9.71	0.036	n/a n/a	1584.90	0.01	0.016	+0.12, -0.10
7.94	-8.01	0.036	n/a n/a	1995.30	0.01	0.016	+0.12, -0.10
10.00	-6.42	0.016	n/a n/a	2511.90	0.01	0.016	+0.12, -0.10
12.59	-4.99	0.016	n/a n/a	3162.30	0.01	0.016	+0.13, -0.10
	-3.75	0.016	n/a n/a	3981.10	0.01	0.016	+0.13, -0.10
15.85	-2.73	0.016	-1.20, -5.00	5011.90	0.00	0.016	+0.14, -0.10
19.95			-0.73, -3.30	6309.60	-0.01	0.016	+0.14, -0.11
25.12	-1.93	0.016	• • • •	7943.30	-0.03	0.016	+0.14, -0.13
31.62	-1.34	0.016	-0.50, -2.20	10000.00	-0.07	0.016	+0.14, -0.16
39.81	-0.92	0.016	-0.32, -1.50			0.016	n/a n/a
50.12	-0.62	0.016	-0.21, -1.05	12589.00	-0.11		
63.10	-0.43	0.016	-0.11, -0.75	15849.00	-0.20	0.016	n/a n/a
79.43	-0.29	0.016	-0.05, -0.52	19953.00	-0.33	0.016	n/a n/a
100.00	-0.20	0.016	+0.00, -0.37	25250.00	-0.54	0.022	n/a n/a
125.89	-0.14	0.016	+0.03, -0.30	31500.00	-0.84	0.022	n/a n/a
158.49	-0.10	0.016	+0.05, -0.25	39750.00	-1.32	0.022	n/a n/a
199.53	-0.07	0.016	+0.07, -0.21	50000.00	-2.00	0.022	n/a n/a
251.19	-0.05	0.016	+0.08, -0.18	63000.00	-2.93	0.047	n/a n/a
316.23	-0.04	0.016	+0.09, -0.16	79500.00	-4.12	0.047	n/a n/a
		0.016	+0.09, -0.14	100000.00	-5.51	0.047	n/a n/a
398.11	-0.03		+0.10, -0.14	126000.00	-7.10	0.063	n/a n/a
501.19	-0.02	0.016	+0.10, -0.12	120000.00	/.10	0.000	

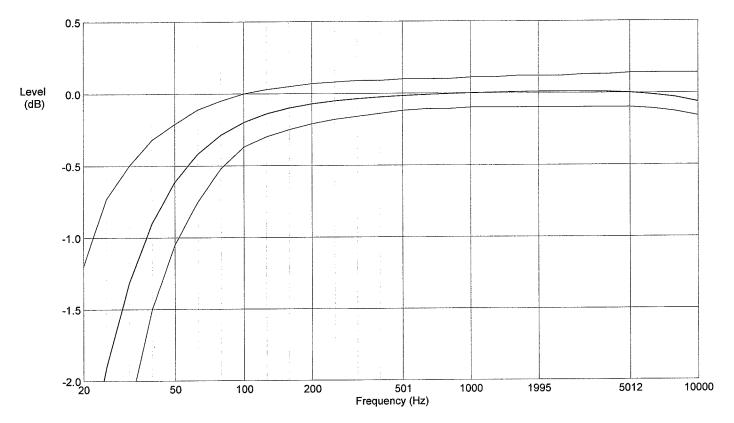
Noise floor data: 1kHz (1/3 Octave) = 0.60 uV, -4.4 dBuV, uncertainty = 0.47 dB Flat (20Hz-20kHz) = 5.0 uV, 13.9 dBuV, uncertainty = 0.47 dB Awt = 2.7 uV, 8.7 dBuV, uncertainty = 0.46 dB

Uncertainties are given as expanded uncertainty at \sim 95% confidence interval (k = 2).

Technician: Jason Grace Test Date: 04AUG2009

Preamplifier Model: 2260-High Serial Number: 0263 Certificate of Electrical Conformance

Frequency response of this model 2260-High preamplifier was tested at a level of 1 Vrms with 18pF microphone capacitance and driving a short cable. Output level at 1kHz is 0.9005 Vrms (-0.910 dBV), uncertainty 0.033 dB. Results are displayed relative to the level at 1kHz.



Freq (Hz)	Measured (dB)	Uncert (dB)	Tolerance (dB)	Freq (Hz)	Measured (dB)	Uncert (dB)	Tolerance (dB)
2.51	-16.94	0.075	n/a n/a	630.96	-0.01	0.016	+0.10, -0.11
3.16	-15.12	0.058	n/a n/a	794.33	-0.01	0.016	+0.10, -0.11
3.98	-13.29	0.058	n/a n/a	1000.00	0.00	0.016	+0.11, -0.10
5.01	-11.46	0.036	n/a n/a	1258.90	0.00	0.016	+0.11, -0.10
6.31	-9.67	0.036	n/a n/a	1584.90	0.01	0.016	+0.12, -0.10
7.94	-7.96	0.036	n/a n/a	1995.30	0.01	0.016	+0.12, -0.10
10.00	-6.37	0.016	n/a n/a	2511.90	0.01	0.016	+0.12, -0.10
12.59	-4.94	0.016	n/a n/a	3162.30	0.01	0.016	+0.13, -0.10
15.85	-3.70	0.016	n/a n/a	3981.10	0.01	0.016	+0.13, -0.10
19.95	-2.69	0.016	-1.20, -5.00	5011.90	0.00	0.016	+0.14, -0.10
25.12	-1.90	0.016	-0.73, -3.30	6309.60	-0.01	0.016	+0.14, -0.11
31.62	-1.32	0.016	-0.50, -2.20	7943.30	-0.03	0.016	+0.14, -0.13
39.81	-0.90	0.016	-0.32, -1.50	10000.00	-0.06	0.016	+0.14, -0.16
50.12	-0.61	0.016	-0.21, -1.05	12589.00	-0.11	0.016	n/a n/a
63.10	-0.42	0.016	-0.11, -0.75	15849.00	-0.20	0.016	n/a n/a
79.43	-0.29	0.016	-0.05, -0.52	19953.00	-0.32	0.016	n/a n/a
100.00	-0.20	0.016	+0.00, -0.37	25250.00	-0.53	0.022	n/a n/a
125.89	-0.14	0.016	+0.03, -0.30	31500.00	-0.83	0.022	n/a n/a
158.49	-0.10	0.016	+0.05, -0.25	39750.00	-1.29	0.022	n/a n/a
199.53	-0.07	0.016	+0.07, -0.21	50000.00	-1.96	0.022	n/a n/a
251.19	-0.05	0.016	+0.08, -0.18	63000.00	-2.88	0.047	n/a n/a
316.23	-0.04	0.016	+0.09, -0.16	79500.00	-4.05	0.047	n/a n/a
398.11	-0.03	0.016	+0.09, -0.14	100000.00	-5.43	0.047	n/a n/a
501.19	-0.02	0.016	+0.10, -0.12	126000.00	-7.01	0.063	n/a n/a

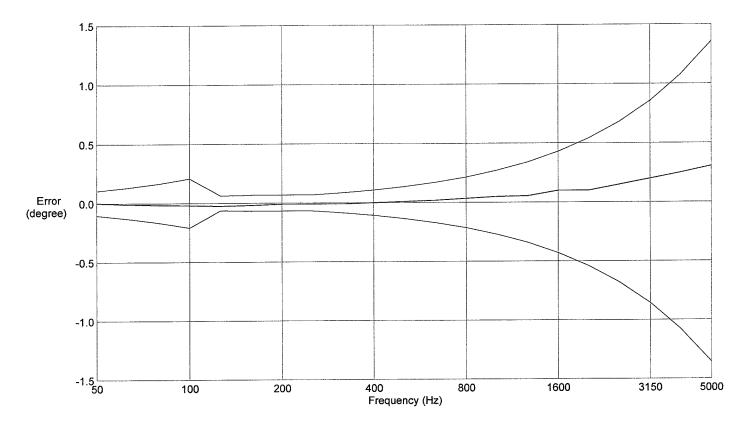
Noise floor data: 1kHz (1/3 Octave) = 0.62 uV, -4.1 dBuV, uncertainty = 0.47 dB Flat (20Hz-20kHz) = 5.2 uV, 14.3 dBuV, uncertainty = 0.47 dB Awt = 2.8 uV, 9.0 dBuV, uncertainty = 0.46 dB

Uncertainties are given as expanded uncertainty at ~95% confidence interval (k = 2).

Technician: Jason Grace Test Date: 04AUG2009

Model: 2260-Phase Serial Number: 0263 CH 1 Mic: 2640 1436 CH 2 Mic: 2640 1345

Phase errors for the probe. This Class 1 Intensity Probe was tested with a Residual-intensity calibrator model CAL 291. This data was taken after the probe was adjusted for phase with the two adjustors on the side of the probe handle.



Freq	Measured	LD Tolerance	Spacer	Freq	Measured	LD Tolerance	Spacer
(Hz)	(degree)	(degree)	(mm)	(Hz)	(degree)	(degree)	(mm)
$\begin{array}{c} 50.12\\ 63.10\\ 79.43\\ 100.00\\ 125.90\\ 158.50\\ 199.50\\ 251.20\\ 316.20\\ 398.10\\ 501.20\end{array}$	$\begin{array}{c} 0.0000\\ -0.0100\\ -0.0150\\ -0.0200\\ -0.0250\\ -0.0200\\ -0.0100\\ -0.0100\\ -0.0100\\ -0.0100\\ 0.0000\\ 0.0100\end{array}$	$\begin{array}{c} +0.1047, -0.1047\\ +0.1318, -0.1318\\ +0.1660, -0.1660\\ +0.2089, -0.2089\\ +0.0631, -0.0631\\ +0.0681, -0.0681\\ +0.0681, -0.0681\\ +0.0681, -0.0681\\ +0.0681, -0.0681\\ +0.0857, -0.0857\\ +0.1079, -0.1079\\ +0.1359, -0.1359\end{array}$	50 12 12 12 12 12 12 12	631.00 794.30 1000.00 1259.00 1585.00 1995.00 2512.00 3162.00 3981.00 5012.00	$\begin{array}{c} 0.0200\\ 0.0350\\ 0.0550\\ 0.1000\\ 0.1000\\ 0.1500\\ 0.2000\\ 0.2500\\ 0.3050\\ \end{array}$	$\begin{array}{c} +0.1711, & -0.1711\\ +0.2153, & -0.2153\\ +0.2711, & -0.2711\\ +0.3413, & -0.3413\\ +0.4297, & -0.4297\\ +0.5409, & -0.5409\\ +0.6810, & -0.6810\\ +0.8574, & -0.8574\\ +1.0800, & -1.0800\\ +1.3590, & -1.3590\end{array}$	12 12 12 12 12 12 12 12

Limits are the smallest of ANSI S1.9-1996 table 7 or IEC 1043-1993 table 2 Class 1.

Technician: Jason Grace Test Date: 04AUG2009



APPENDIX G

Measurements

(Measured sound pressure level (L_{EQ}) in one third octave band format is given in this appendix. The data are given in dB re 20 x 10⁻⁶ Pa. The measurements were taken as a scan of the surface)



Frequency (Hz)	Transformer	Transformer	Transformer	Xantrex Intake	Xantrex Exhaust	Xantrex Cooling1	Xantrex Cooling2	SMA intake	SMA exhaust
25	51	52	51	72	75	68	70	55	69
31.5	52	55	52	66	72	63	68	55	69
40	50	51	50	62	70	65	68	59	76
50	50	53	51	59	69	64	67	62	75
63	56	58	58	65	67	67	70	58	74
80	51	48	45	65	66	69	71	55	73
100	53	50	44	66	65	69	71	55	71
125	56	55	58	73	73	72	73	61	66
160	46	41	37	68	70	70	70	55	65
200	55	45	39	70	65	72	73	51	63
250	53	54	51	74	66	71	75	56	69
315	51	48	45	74	74	72	78	64	76
400	51	50	47	72	78	70	73	57	74
500	52	51	44	70	69	68	70	61	70
630	46	47	41	69	69	68	70	56	71
800	47	46	37	74	69	74	76	52	66
1000	50	40	36	65	66	67	70	53	63
1250	44	38	35	69	67	68	73	54	68
1600	45	38	35	69	67	67	72	54	67
2000	41	35	34	63	66	64	71	52	63
2500	45	37	39	60	64	62	69	54	71
3150	48	37	44	58	63	59	67	55	75
4000	32	33	28	56	61	57	65	46	59
5000	36	42	40	61	58	59	66	45	57
6300	43	39	40	78	62	76	81	55	70
8000	34	34	34	59	52	59	66	42	56
10000	34	31	29	50	44	51	55	41	55



APPENDIX H

Weather Data



Weather Data

Source: Environment Canada, Climate Data Online, <u>www.climate.weatheroffice.ec.gc.ca/climateData/canada_e.html</u> LONDON INT'L AIRPORT Station:

Latitude: 43° 1.8' N Longitude: 82° 9' W

Date/Time	Time	Temp (°C)	Dew Point Temp (°C)	Rel Hum (%)	Wind Dir (10's deg)	Wind Spd (km/h)	Visibility (km)	Stn Press (kPa)	Wind Chill	Weather
8/6/2010	0:00	19	15	78	34	13	24	97.61		Clear
8/6/2010	1:00	18	15	81	29	6	24	97.65		Clear
8/6/2010	2:00	17	14	84	32	4	24	97.67		Mainly Clear
8/6/2010	3:00	17	14	81	29	7	24	97.67		Mostly Cloudy
8/6/2010	4:00	18	12	68	32	7	24	97.68		Mainly Clear
8/6/2010	5:00	17	12	71	34	6	24	97.74		Mostly Cloudy
8/6/2010	6:00	17	12	73	32	4	24	97.76		Mostly Cloudy
8/6/2010	7:00	18	13	71	31	6	24	97.81		Mainly Clear
8/6/2010	8:00	19	12	62	35	9	24	97.85		Mostly Cloudy
8/6/2010	9:00	20	12	60	28	7	24	97.90		Mainly Clear
8/6/2010	10:00	22	12	52	28	7	24	97.90		Mostly Cloudy
8/6/2010	11:00	22	12	53	29	13	24	97.92		Mostly Cloudy
8/6/2010	12:00	23	15	62	26	15	24	97.91		Mostly Cloudy
8/6/2010	13:00	23	13	52	27	17	24	97.86		Mostly Cloudy
8/6/2010	14:00	24	13	50	27	17	24	97.82		Mostly Cloudy
8/6/2010	15:00	24	14	53	28	24	24	97.81		Mostly Cloudy
8/6/2010	16:00	24	14	54	31	15	24	97.81		Mostly Cloudy
8/6/2010	17:00	24	14	54	31	15	24	97.86		Mostly Cloudy
8/6/2010	18:00	22	13	55	31	13	24	97.87		Mainly Clear
8/6/2010	19:00	21	12	58	33	17	24	97.92		Mainly Clear
8/6/2010	20:00	19	11	62	26	11	24	97.99		Mainly Clear
8/6/2010	21:00	17	11	67	1	7	24	98.10		Mainly Clear
8/6/2010	22:00	16	11	71	36	6	24	98.12		Clear
8/6/2010	23:00	14	11	78	3	9	24	98.15		Clear

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